Technical Document RA21043

.

. — Technical Requirements



CB USE ONLY	Application number	Legal land description					
Approval Registration Authorization	RA21043	NE 15-42-24 W4M					
APPLICATION DISCLOSURE							
This information is collected under the authority of the Agorovisions of the Freedom of Information and Protection of written request that certain sections remain private.	ricultural Operation Practices A of Privacy Act. This information	ct (AOPA), and is subject to the is public unless the NRCB grants a					
Any construction prior to obtaining an NRCB permit prosecution.	is an offence and is subject	to enforcement action, including					
, the applicant, or applicant's agent, have read and unde provided in this application is true to the best of my know	erstand the statements above, a vledge.	nd I acknowledge that the information					
Feb 18/22	hit	ala.					
Date of signing	Signature	alla -					
Double T Cattle	Joe Thalen						
Corporate name (if applicable)	Print name	Print name					
CENERAL INCORMATION REQUIREMENTS							
GENERAL INFORMATION REQUIREMENTS Proposed facilities: list all proposed confined feeding proposed facilities are additions to existing facilities. (at							
Proposed facilities		Dimensions (m) (length, width, and depth)					
6 feedlot pens Total Area 52,256 sq. m with		4-32.97x304.8 & 2-32.97x182.8					
Total area under roof 15,057 sq. m (scraper alley a	nd feed alley)	4-9.5x304.8 & 2-9.5x182.88					
	43mx110x & 52mx34m-						
Catch basin 'L' shaped Refer to dro	wing for exact	Approx					
Catch basin 'L' shaped Refer to dre Size -	wing for exact	56.64 × 122.38 38.61 × 52.21					

Existing facilities	Dimensions (m) (length, width, and depth)	NRCB USE ONLY		
Sow Barn	27mx40m			
Note: only the approximate east half of the though the north pit wall was renovated to is further discussed on the next page and i	include drive through overhead	doors. This barr		
NRCB USE ONLY				

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Part 2 — Technical Requirements



Application under the Agricultural Operation Practices Act for a confined feeding operation, manure collection area, and/or manure storage facility(ies)

new facility is replacing an old facility, please explain what will happen to the old facility and when.	☑ N/A
d pig barn is being used for livestock processing building.	
ivestock processing facilities are not considered to be manure collection areas or nanure storage facilities; they are ancillary structures that do not require a permit unde ne AOPA.	÷r

Construction completion date for proposed facilities

Additional information

Livestock numbers: Complete only if livestock numbers are different from what was identified in the Part 1 application. Note: if livestock numbers increase in your Part 2 application, a new Part 1 application must be submitted which may result in a loss of priority for minimum distance separation (MDS).

Livestock category and type (Available in the Schedule 2 of the Part 2 Matters Regulation)	Permitted number	Proposed increase or decrease in number (if applicable)	Total
Beef, Cow/finisher	0	4500	4500
Sow Farrow to Finish	700	700	0
The status of the CFO's permits and its Summary RA21043.	associated livesto	ck capacity are disc	ussed in Decision
		Technical Document R	A21043 Page 2 of 83





	rt 2 — Technical Requirements ation under the Agricultural Operation Practices Act for a confined feeding op	
	ECLARATION AND ACKNOWLEDGMENT OF AI	PPLICANT CONCERNING WATER ACT LICENCE AEP) for a confined feeding operation (CFO) the following four options
OPT	I DO want my water licence application coupled to my AOPA p	ermit and the Water Act licence permit application.
Signe	ed thisday of, 20	Signature of Applicant or Agent
OPT	ION 2: Processing the AOPA permit and Water Act licence	ce separately
1.	I (we) acknowledge that the CFO will need a new water licence	ce from AEP under the Water Act for the development or activity
2.		ndependently of AEP's processing of the CFO's application for a
з.	water licence. In making this request, I (we) recognize that, if this AOPA ap considered by AEP as improving or enhancing the CFO's eligib	oplication is granted by the NRCB, the NRCB's decision will not be bility for a water licence under the <i>Water Act</i> .
	I (we) acknowledge that any construction or actions to popula absence of a <i>Water Act</i> licence will not be relevant to AEP's c	late the CFO with livestock pursuant to an AOPA permit in the consideration of whether to grant the <i>Water Act</i> licence application
	I (we) acknowledge that any such construction or livestock poly application is denied or if the operation of the CFO is otherwise being required to depopulate the CFO and/or to cease further in the Water Act).	bopulating will be at the CFO's sole risk if the <i>water Act</i> literice ise deemed to be in violation of the <i>Water Act</i> . This risk includes in construction, or to remove "works" or "undertakings" (as defined
	AS RELEVANT: I (we) acknowledge that the CFO is located i Bow, Oldman and South Saskatchewan River Basin Water Allo to new surface water allocations.	in the South Saskatchewan River Basin and that, pursuant to the location Order [Alta. Reg. 171/2007], this basin is currently closed
Sign	ed this 18 day of FEG, 2022	Signature of Applicant or Agent
1.	ION 3: Additional water licence not required I (we) declare that the CFO will not need a new licence from in this AOPA application. ed this day of, 20	AEP under the Water Act for the development or activity proposed
		Signature of Applicant or Agent
1.	activity proposed in this AOPA application.	e is needed from AEP under the <i>Water Act</i> for the development of
2.	and the CEO's application for a water licence	e NRCB process the AOPA application independently of AEP's
3.	In making this request, I (we) recognize that, if this AOPA at considered by AEP as improving or enhancing the CEO's eligi	pplication is granted by the NRCB, the NRCB's decision will not be ibility for a water licence under the <i>Water Act</i> .
4.	I (we) acknowledge that any construction or actions to populate in the absence of a <i>Water Act</i> licence will not be relevant to application. If a new water licence is needed.	Ilate the CFO with additional livestock pursuant to an AOPA permit AEP's consideration of whether to grant my <i>Water Act</i> licence
5.	I (we) acknowledge that any such construction or livestock i application is denied or if the operation of the CFO is otherw being required to depopulate the CFO and/or to cease further in the Water Art).	increase will be at the CFO's sole risk if the <i>Water Act</i> licence vise deemed to be in violation of the <i>Water Act</i> . This risk includes er construction, or to remove "works" or "undertakings" (as define
6.	AC PELEVANT: I (we) acknowledge that the CFO is located	I in the South Saskatchewan River Basin and that, pursuant to the <i>Mocation Order</i> [Alta. Reg. 171/2007], this basin is currently closed

Signed this _____ day of ____ , 20____

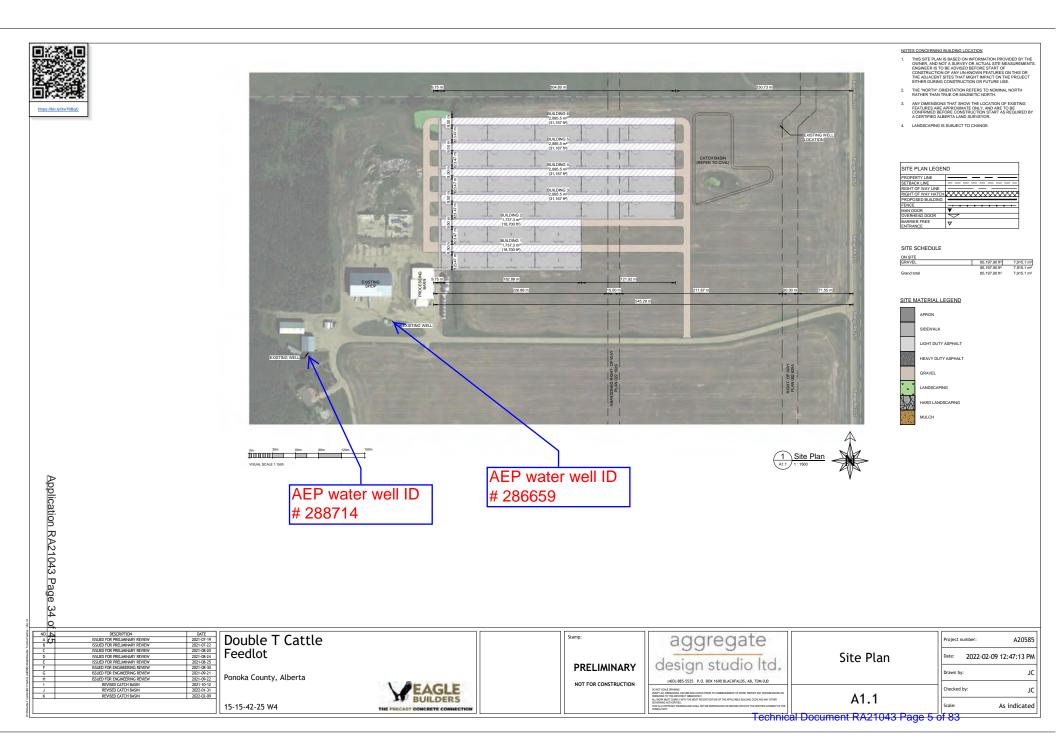
Signature of Applicant or Agent

to new surface water allocations.





NRCB USE ONLY							
ALL SIGNATURES	IN FILE	XYES [ОИС				
DATES OF APPROV	AL OFFICER SITE V	/ISITS					
December 17, 202	21, March 24 and 30,	, 2022					
		ITIES AN		RAL A	GENCIE	S	
Date deeming letters sen							
Municipality:							
Letter sent	response received	🗴 writter	n/email		verbal		no comments received
Alberta Health Services	s:						
Ietter sent	I response received	🛛 writter	n/email		verbal		no comments received
Alberta Environment a	nd Parks: N/A						
🔽 letter sent	I response received	🗴 writter	n/email		verbal		no comments received
Alberta Transportation	:: 🛛 N/A						
Letter sent	☐ response received	🔲 writter	n/email		verbal		no comments received
Alberta Regulatory Ser	vices: X N/A						
Letter sent	□ response received	uritter	n/email		verbal		no comments received
Other:					Č i	N/A	
Letter sent	□ response received	writter	n/email		verbal		no comments received
Other:						NI / A	
other:						N/A	
Letter sent	□ response received	written	n/email		verbal		no comments received
	e responses to the ap Transportation, Albe 3.						



Alberta

Water Well Drilling Report

The driller supplies the data contained in this report. The Province disclaims responsibility for its accuracy. The information on this report will be retained in a public database. View in Metric Export to Excel

GIC Well ID 2 GoA Well Tag No. Drilling Company Well ID

288714

WN ID		a	ccuracy. The in	nformation or	this report will be r	retained in a p	ublic databas	Se.		Date Report Received	1997/11/06
Well Ident	ification and L	ocation								Me	asurement in Imperia
Owner Name Address VAN DEPT, WIM RR3, PONOKA				IOKA	Town				Province	Country	Postal Code T4L 1R3
Location	1/4 or LSD NE	SEC 15	TWP 42	RGE 25	W of MER 4	Lot	Block	Plan	Addition	al Description	
Measured i	-	of ft from ft from	_		GPS Coordin Latitude 5 How Location Not Verified	2.620020		es (NAD 83 tude <u>-113.</u> t	10 A A A A A A A A A A A A A A A A A A A	Elevation How Elevation Obtained	ft ed

Formation Log		Measurement in Imperial	Yield Test Sur	nmary	1		Meas	urement in Imperi
Depth from	Water	Lithology Description	All Provide and a second s		ate25.0			
ground level (ft)	Bearing		Test Date	Wate	r Removal Rate (igpm)	Static	Water Level (ft)
20.00		Brown Shale	1997/09/14		25.00			162.00
115.00	1	Gray Shale	Well Completie					urement in Imperi
120.00		Sand & Coal	300.00 ft	ed Fini	ished Well Depth	Start Date 1997/09/		End Date 1997/09/11
150.00		Shale	Borehole			1001100/	10	1007100/11
155.00	1	Gray Sandstone	Diameter	(in)	From	(#)	-	To (ft)
170.00	-	Gray Shale	0.00	(11)	0.		1	300.00
172.00		Hard Shale	Surface Casing	(if app	licable)	Well Casin	g/Liner	
217.00	-	Gray Sandstone	Plastic		6 00 i-	Plastic		1.50 1-
255.00		Gray Shale	Wall Thickness	_	6.00 in 0.039 in			4.50 in 0.237 in
260.00	1	Coal	apprent production and		139.00 ft			120.00 ft
280.00		Gray Shale	Dollom a		155.00 11		om at :	
290.00		Coal	Perforations			Don	-	
			280.00 S Perforated by Annular Seal Placed from Amount Other Seals Screen Type Size OL From (f Attachmer Top Fitting Pack	C Type D: t) ot s	0.00 ft to	- (ft)	At ittings	8.00 0.00 (ft) Slot Size (in)

TALL PINE DRILLING LTD.

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Alberta

GOWN ID

Water Well Drilling Report

The driller supplies the data contained in this report. The Province disclaims responsibility for its accuracy. The information on this report will be retained in a public database. View in Metric Export to Excel

GIC Well ID 288714 GoA Well Tag No. Drilling Company Well ID Date Report Received 1997/11/06

ven idenui	fication and L	ocation									Measurement in Imp
Owner Name /AN DEPT, \			Address RR3, PON	ОКА		Tov	vn		Province	Coun	try Postal Coo T4L 1R3
ocation	1/4 or LSD NE	SEC 15	TWP 42	RGE 25	W of MER 4		Block	Plan	0.0700000	nal Description	
Aeasured fro	om Boundary o	of					ecimal Degre			Phonethea	
		ft from) Long	itude -113.	5180/1		ft
		ft from		1.1	How Loca Not Verifie	tion Obtaine	d			How Elevation Not Obtained	Obtained
dditional I	Information				1101 1011					1101 0 2 100/04	Measurement in Imp
					15						measurement in imp
	rom Top of Cas n Flow				10	-	Is Flow Co	ntrol Installe	d		
10 / 11001011	Rate		igpm						9		
	ded Pump Rat	I martine and the second se			25.00 ig	pm Pu	mp Installed	Yes			ft
	ded Pump Inta		(From TOC)		270.00 ft	T	/De		Make	a ra con	H.P. 3
r coourninoin	dou'r anip ma	no Dopart	(110)/1100)		2,0,00 11	- 3				Model (Outpu	ut Rating)
Did you E	Encounter Salin	e Water (>	>4000 ppm TI	DS)	De	oth	ft	Well Disi	nfected Upon	Completion	
Did Joa L			Ciana Print 1	Gas	De	oth	ft	Ge	onhysical I o	g Taken	-
						pu1		00	Submitted to		
									Submitted to	LOND	
112010100100	al Comments o	a categorie a sub-					Sample C	Collected for	Potability	S	Submitted to ESRD
112010100100	al Comments o REPORTS DIS	a categorie a sub-	ROM TOP OF	CASING	TO GROUNE) LEVEL: 1'.	Sample C		ken From 0	Ground Level	Submitted to ESRD
DRILLER R /ield Test		TANCE FF					Sample C		ken From 0		
DRILLER R	REPORTS DIS	a categorie a sub-	ne		TO GROUNE ic Water Leve 162.00 ft	1			iken From (Depl	Ground Level h to water level Elapsed Time	
DRILLER R 'ield Test Test Date	REPORTS DIS	TANCE FF	ne		ic Water Leve	1		Ta	iken From (Depl	Ground Level h to water level	Measurement in Imp
DRILLER R Yield Test Test Date 1997/09/14	REPORTS DIS	Start Tim 12:00 AM	ne		ic Water Leve	1		Ta	iken From (Depl	Ground Level h to water level Elapsed Time Minutes:Sec	Measurement in Imp Recovery (ft) 188.00 174.00
DRILLER R 'ield Test Test Date 1997/09/14	REPORTS DIS	Start Tin 12:00 AM	ne		ic Water Leve	1		Ta	iken From (Depl	Ground Level h to water level Elapsed Time Minutes:Sec 1:00 2:00 3:00	Measurement in Imp Recovery (ft) 188,00 174,00 170,00
DRILLER R 'ield Test Test Date 1997/09/14 Method of I	REPORTS DIS [®] Water Remov Type <u>F</u> emoval Rate	Start Tim 12:00 AM	ne M 25.00 japm		ic Water Leve	1		Ta	iken From (Depl	Ground Level h to water level Elapsed Time Minutes:Sec 1:00 2:00 3:00 4:00	Measurement in Imp Recovery (ft) 188.00 174.00 170.00 168.00
DRILLER R field Test Test Date 1997/09/14 Method of I	REPORTS DIS [®] Water Remov Type <u>F</u> emoval Rate	Start Tim 12:00 AM	ne M 25.00 japm		ic Water Leve	1		Ta	iken From (Depl	Ground Level h to water level Elapsed Time Minutes:Sec 1:00 2:00 3:00 4:00 5:00	Measurement in Imp Recovery (ft) 188.00 174.00 170.00 168.00 167.00
DRILLER R 'ield Test Test Date 1997/09/14 Method of I	REPORTS DIS Water Remov Type <u>F</u>	Start Tim 12:00 AM	ne M 25.00 japm		ic Water Leve	1		Ta	iken From (Depl	Ground Level h to water level clapsed Time Minutes:Sec 1:00 2:00 3:00 4:00 5:00 6:00	Measurement in Imp Recovery (ft) 188.00 174.00 170.00 168.00 166.00
DRILLER R field Test Test Date 1997/09/14 Method of I Re Depth With	Water Remov Type E emoval Rate adrawn From	Start Tim 12:00 AN Pump 2	ne M 25.00 igpm 270.00 ft	Stat	ic Water Leve	1		Ta	iken From (Depl	Ground Level h to water level Elapsed Time Minutes:Sec 1:00 2:00 3:00 4:00 5:00 6:00 7:00	Measurement in Imp Recovery (ft) 188.00 174.00 170.00 168.00 165.00 165.50
DRILLER R Field Test Test Date 1997/09/14 Method of I Re Depth With	REPORTS DIS [®] Water Remov Type <u>F</u> emoval Rate	Start Tim 12:00 AN Pump 2	ne M 25.00 igpm 270.00 ft	Stat	ic Water Leve	1		Ta	iken From (Depl	Cround Level h to water level Elapsed Time Minutes:Sec 1:00 2:00 3:00 4:00 5:00 6:00 7:00 8:00	Measurement in Imp Recovery (ft) 188.00 174.00 170.00 168.00 165.50 165.00
DRILLER R field Test Test Date 1997/09/14 Method of I Re Depth With	Water Remov Type E emoval Rate adrawn From	Start Tim 12:00 AN Pump 2	ne M 25.00 igpm 270.00 ft	Stat	ic Water Leve	1		Ta	iken From (Depl	Ground Level h to water level Elapsed Time Minutes:Sec 1:00 2:00 3:00 4:00 5:00 6:00 7:00 8:00 9:00	Measurement in Imp Recovery (ft) 188.00 174.00 170.00 168.00 167.00 165.50 165.50 164.58
DRILLER R field Test Test Date 1997/09/14 Method of I Re Depth With	Water Remov Type E emoval Rate adrawn From	Start Tim 12:00 AN Pump 2	ne M 25.00 igpm 270.00 ft	Stat	ic Water Leve	1		Ta	iken From (Depl	Cround Level h to water level Elapsed Time Minutes:Sec 1:00 2:00 3:00 4:00 5:00 6:00 7:00 8:00	Measurement in Imp Recovery (ft) 188.00 174.00 170.00 168.00 165.50 165.00
DRILLER R /ield Test Test Date 1997/09/14 Method of I Re Depth With	Water Remov Type E emoval Rate adrawn From	Start Tim 12:00 AN Pump 2	ne M 25.00 igpm 270.00 ft	Stat	ic Water Leve	1		Ta	iken From (Depl	Ground Level h to water level Elapsed Time Minutes:Sec 1:00 2:00 3:00 4:00 5:00 6:00 7:00 8:00 9:00 10:00	Measurement in Imp Recovery (ft) 188.00 174.00 170.00 168.00 165.00 165.50 165.80 164.58 164.67
DRILLER R /ield Test Test Date 1997/09/14 Method of I Re Depth With	Water Remov Type E emoval Rate adrawn From	Start Tim 12:00 AN Pump 2	ne M 25.00 igpm 270.00 ft	Stat	ic Water Leve	1		Ta	iken From (Depl	Cround Level h to water level Elapsed Time Minutes:Sec 1:00 2:00 3:00 4:00 5:00 6:00 7:00 8:00 9:00 10:00 14:00 20:00 35:00	Measurement in Imp Recovery (ft) 188.00 174.00 170.00 168.00 167.00 165.50 165.50 164.58 164.67 163.58 162.08
DRILLER R /ield Test Test Date 1997/09/14 Method of I Re Depth With	Water Remov Type E emoval Rate adrawn From	Start Tim 12:00 AN Pump 2	ne M 25.00 igpm 270.00 ft	Stat	ic Water Leve	1		Ta	iken From (Depl	Bround Level h to water level Elapsed Time Minutes:Sec 1:00 2:00 3:00 4:00 5:00 6:00 7:00 8:00 9:00 10:00 14:00 20:00	Measurement in Imp Recovery (ft) 188.00 174.00 170.00 168.00 167.00 165.50 165.50 164.58 164.67 163.58 162.08
DRILLER R field Test Test Date 1997/09/14 Method of R Re Depth With	Water Remov Type <u>F</u> emoval Rate _ ndrawn From _	TANCE FF Start Tim 12:00 AN Pump 2 2 as < 2 hour	ne M 25.00 igpm 270.00 ft	Stat	ic Water Leve	1		Ta	iken From (Depl	Cround Level h to water level Elapsed Time Minutes:Sec 1:00 2:00 3:00 4:00 5:00 6:00 7:00 8:00 9:00 10:00 14:00 20:00 35:00	Measurement in Imp Recovery (ft) 188.00 174.00 170.00 168.00 167.00 165.50 165.50 164.58 164.67 163.58 162.08
DRILLER R Field Test Test Date 1997/09/14 Method of R Re Depth With	Water Remov Type E emoval Rate ndrawn From noval period wa	TANCE FF Start Tim 12:00 AN Pump 2 2 as < 2 hour	ne M 25.00 igpm 270.00 ft	Stat.	ic Water Leve	1		Ta	iken From (Depi	Cround Level h to water level Elapsed Time Minutes:Sec 1:00 2:00 3:00 4:00 5:00 6:00 7:00 8:00 9:00 10:00 14:00 20:00 35:00	Measurement in Imp Recovery (ft) 188.00 174.00 170.00 168.00 167.00 165.50 165.00 164.58 164.67 163.58 162.08

Contractor Certification		
Name of Journeyman responsible for drilling/construction of well UNKNOWN NA DRILLER	Certification No 1	
Company Name TALL PINE DRILLING LTD.	Copy of Well report provided to owner	Date approval holder signed
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Abertan Water Well Drilling Report

The driller supplies the data contained in this report. The Province disclaims responsibility for its accuracy. The information on this report will be retained in a public database.

View in Metric Export to Excel

GIC Well ID GoA Well Tag No. Drilling Company Well ID Date Report Received 1997/06/23

286659

DWN ID		a	ccuracy. The i	nformation or	this report will be r	retained in a p	ublic databas	se.		Date Report Received	1997/06/23
Well Ident	ification and L	ocation	15-5-							Me	easurement in Imperia
Owner NameAddressVAN DE PAL, WIMP.O. BOX 6 SITE 19				6 SITE 19	<i>Town</i> RR3, PONOKA				Province	Country	Postal Code T4L 1R3
Location	1/4 or LSD NE	SEC 15	TWP 42	RGE 25	W of MER 4	Lot	Block	Plan	Additio	nal Description	
Measured t	-	of ft from ft from	_		GPS Coordin Latitude 5 How Location Not Verified	52.620020		es (NAD 83 itude <u>-113.</u>	Contraction of the second	Elevation How Elevation Obtain Not Obtained	ft ed

Formation Log		Meas	surement in Imperial	Yield Test Sur	nmary			Mea	surement in Im
Depth from	Water	Lithology Description		Recommended	Pump R	ate 15.0	0 igpm		
ground level (ft)	Bearing	A CONTRACTOR OF A		Test Date		r Removal Rate (Statio	c Water Level (ft)
20.00		Clay		1997/04/29		15.00			168.80
40.00		Gray Sand		Well Completie		Sector Sector			surement in Im
50.00	-	Gray Shale			led Fini	shed Well Depth			End Date
60.00		Hard Sandstone		270.00 ft			1997/	J4/29	1997/04/29
110.00	1	Gray Shale		Borehole		-	103		
120.00		Green Shale		Diameter 0.00	(in)	From 0.1	n (ft) 20	-	To (ft) 270.00
130.00		Gray Sandstone		Surface Casing	(if app			sing/Liner	
170.00	1	Green Shale		Plastic			Plastic		
250.00		Gray Sandstone				6.00 in			4.50 in
270.00		Green Shale		Wall Thickness		0.039 in 79.00 ft	Wall T.		0.237 in
				Bottom a		79.00 π		ottom at :	70.00 ft 270.00 ft
					Driven 0	.00 ftto	79,00		: (ft)
				Screen Type Size OD	»:	0.00 in			
				From (f		To	(ft)	-	Slot Size (in)
				Attachmen Top Fitting	-		Bottor	n Fittings	
				Pack Type Amount			Grain	Size	

Name of Journeyman responsible for drilling/construction of well UNKNOWN NA DRILLER

Company Name TALL PINE DRILLING LTD. Certification No 1

Copy of Well report provided to owner Date approval holder signed

Printed on 9/7/2021 12:49:46 PM

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Albertan Water Well Drilling Report

The driller supplies the data contained in this report. The Province disclaims responsibility for its

View in Metric Export to Excel

GIC Well ID 286659 GoA Well Tag No. Drilling Company Well ID

Vell Identificat											Date Report Rece	siveu n	
	tion and L	ocation										Measur	ement in Imp
Owner Name			Address				Town			Province	Countr		Postal Cod
AN DE PAL, W	VIM		P.O. BOX	SITE 19	RR3, PON	IOKA				1.41.004			T4L 1R3
	4 or LSD	SEC 15	TWP 42	RGE 25	W of M 4	<i>MER</i>	Lot	Block	Plan	Additio	nal Description		
Aeasured from E						Coordina	ates in Dec.	imal Degre	es (NAD 83	8) 1			
incuburbu nom E		ft from			Latitud	le 52	2.620020	Long	itude -113.5	518071	Elevation		ft
-		ft from			How L	ocation	Obtained				How Elevation C	Obtained	
-		It from			Not Ve						Not Obtained		
dditional Infor	rmation					-						Measur	ement in Imp
Distance From	Top of Casi	ing to Groui	nd Level		ir	n							
Is Artesian Flow	w					-	1	s Flow Con	trol Installed	d			
Rat	te		igpm						Describe	e			
Recommended	Pump Rate	9		-	15.00	igpm	Pump	Installed			Depth	ft	
Recommended	Pump Intal	ke Depth (F	rom TOC)				Type		-	Make		HP.	-
	, and a near	in a shart fr		-	200100		1)40	-		mane	Model (Output	Rating)	
Did you Encou	unter Saline	o Water (>4	1000 pom T	(20		Denth		ft	Wall Disi	nfacted Linon	Completion		
Bid you Elicot	unter ounne	, mater let				Depth							
			4	Gas		Depin.		π	Geo	and the second second	g Taken		
Additional Co					TO GROU			Sample C	ollected for i	Submitted to		bmitted to E	SRD
DRILLER REPC					TO GROU	IND LE		Sample C		Potability	Su		
DRILLER REPC	ORTS DIST	ANCE FRO	DM TOP OF	CASING				Sample C		Potability			SRD
DRILLER REPC /ield Test <i>Test Date</i>	ORTS DIST		DM TOP OF	CASING	TO GROU ic Water Le 168.80	evel				Potability	Su Su	Measure	
DRILLER REPO field Test Test Date 1997/04/29	ORTS DIST	Start Time	DM TOP OF	CASING	ic Water Le	evel			Та	Potability	Sround Level h to water level Elapsed Time Minutes:Sec 1:00	Measure	ement in Imp covery (ft) 189.00
DRILLER REPO ield Test Test Date 1997/04/29	ORTS DIST	Start Time 12:00 AM	DM TOP OF	CASING	ic Water Le	evel			Та	Potability	Sround Level h to water level Elapsed Time Minutes:Sec 1:00 2:00	Measure	ement in Imp covery (ft) 189.00 177.00
DRILLER REPO ield Test Fest Date 997/04/29	ORTS DIST	Start Time 12:00 AM	DM TOP OF	CASING	ic Water Le	evel			Та	Potability	Sround Level h to water level Elapsed Time Minutes:Sec 1:00 2:00 3:00	Measure	ement in Imp covery (ft) 189.00 177.00 174.50
DRILLER REPO leld Test Fest Date 997/04/29 Alethod of Wate	ORTS DIST ter Remova Type <u>A</u>	Start Time 12:00 AM	DM TOP OF	CASING	ic Water Le	evel			Та	Potability	Sround Level h to water level Elapsed Time Minutes:Sec 1:00 2:00 3:00 4:00	Measure	ement in Imp covery (ft) 189.00 177.00 174.50 173.50
DRILLER REPO Teld Test Test Date 997/04/29 Method of Wate Remov	ORTS DIST ter Remova Type <u>A</u> oval Rate	Start Time 12:00 AM al 15	DM TOP OF	CASING	ic Water Le	evel			Та	Potability	Sround Level h to water level Elapsed Time Minutes:Sec 1:00 2:00 3:00 4:00 5:00	Measur	ement in Imp covery (ft) 189.00 177.00 174.50 173.50 173.25
DRILLER REPO Teld Test Test Date 997/04/29 Method of Wate Remov	ORTS DIST ter Remova Type <u>A</u> oval Rate	Start Time 12:00 AM al 15	DM TOP OF	CASING	ic Water Le	evel			Та	Potability	Sub Sround Level h to water level Elapsed Time Minutes:Sec 1:00 2:00 3:00 4:00 5:00 7:00	Measur	ement in Imp overy (ft) 189.00 177.00 174.50 173.50 173.25 172.58
RILLER REPC eld Test est Date 997/04/29 fethod of Wate Remov Depth Withdraw	ter Remova Type A oval Rate wn From	Start Time 12:00 AM al .ir 15 208	DM TOP OF	^c CASING	ic Water Le	evel			Та	Potability	Sub Sround Level h to water level Elapsed Time Minutes:Sec 1:00 2:00 3:00 4:00 5:00 7:00 8:00	Rec	ement in Imp sovery (ft) 189.00 177.00 174.50 173.25 172.58 172.33
RILLER REPC eld Test est Date 997/04/29 fethod of Wate Remov Depth Withdraw	ter Remova Type A oval Rate wn From	Start Time 12:00 AM al .ir 15 208	DM TOP OF	^c CASING	ic Water Le	evel			Та	Potability	Sub Sround Level h to water level Elapsed Time Minutes:Sec 1:00 2:00 3:00 4:00 5:00 7:00 8:00 10:00	Rec	ement in Imp tovery (ft) 189.00 177.00 174.50 173.50 173.52 172.58 172.58 172.33 171.83
RILLER REPC eld Test est Date 997/04/29 fethod of Wate Remov Depth Withdrav	ter Remova Type A oval Rate wn From	Start Time 12:00 AM al .ir 15 208	DM TOP OF	^c CASING	ic Water Le	evel			Та	Potability	Sround Level h to water level Elapsed Time Minutes:Sec 1:00 2:00 3:00 4:00 5:00 7:00 8:00 10:00 14:00	Rec	ement in Imp covery (ft) 189.00 177.00 174.50 173.50 173.25 172.58 172.33 171.83 171.42
RILLER REPC eld Test est Date 997/04/29 fethod of Wate Remov Depth Withdraw	ter Remova Type A oval Rate wn From	Start Time 12:00 AM al .ir 15 208	DM TOP OF	^c CASING	ic Water Le	evel			Та	Potability	Sub Sround Level h to water level Elapsed Time Minutes:Sec 1:00 2:00 3:00 4:00 5:00 7:00 8:00 10:00 14:00 20:00	Rec	ement in Imp covery (ft) 189.00 177.00 174.50 173.50 173.25 172.58 172.58 172.33 171.83 171.42 170.00
DRILLER REPO ield Test Fest Date 997/04/29 Aethod of Wate Remov Depth Withdraw	ter Remova Type A oval Rate wn From	Start Time 12:00 AM al .ir 15 208	DM TOP OF	^c CASING	ic Water Le	evel			Та	Potability	Su Sround Level h to water level Elapsed Time Minutes:Sec 1:00 2:00 3:00 4:00 5:00 7:00 8:00 10:00 14:00 20:00 30:00	Rec	ement in Imp covery (ft) 189.00 177.00 174.50 173.50 173.25 172.58 172.33 171.83 171.42 170.00 169.75
DRILLER REPO ield Test Fest Date 1997/04/29 Wethod of Wate Remov Depth Withdraw	ter Remova Type A oval Rate wn From	Start Time 12:00 AM al .ir 15 208	DM TOP OF	^c CASING	ic Water Le	evel			Та	Potability	Sub Sround Level h to water level Elapsed Time Minutes:Sec 1:00 2:00 3:00 4:00 5:00 7:00 8:00 10:00 14:00 20:00 30:00 40:00	Rec	ement in Imp tovery (ft) 189.00 177.00 174.50 173.25 172.58 172.33 171.83 171.83 171.42 170.00 169.75 169.42
DRILLER REPO ield Test Test Date 1997/04/29 Wethod of Wate Remov Depth Withdraw	ter Remova Type A oval Rate wn From	Start Time 12:00 AM al .ir 15 208	DM TOP OF	^c CASING	ic Water Le	evel			Та	Potability	Sub Sround Level h to water level Elapsed Time Minutes:Sec 1:00 2:00 3:00 4:00 5:00 7:00 8:00 10:00 14:00 20:00 30:00 40:00 60:00	Rec	ement in Imp tovery (ft) 189.00 177.00 174.50 173.50 173.55 172.58 172.58 172.33 171.83 171.42 170.00 169.75 169.42 169.17
DRILLER REPO (ield Test Test Date 1997/04/29 Method of Wate	ter Remova Type A oval Rate wn From	Start Time 12:00 AM al .ir 15 208	DM TOP OF	^c CASING	ic Water Le	evel			Та	Potability	Sub Sround Level h to water level Elapsed Time Minutes:Sec 1:00 2:00 3:00 4:00 5:00 7:00 8:00 10:00 14:00 20:00 30:00 40:00 90:00	Rec	ement in Imp covery (ft) 189.00 177.00 174.50 173.50 173.25 172.33 171.83 171.42 170.00 169.75 169.42 169.17 168.92
DRILLER REPO Vield Test Test Date 1997/04/29 Method of Wate Remov Depth Withdraw	ter Remova Type A oval Rate wn From	Start Time 12:00 AM al .ir 15 208	DM TOP OF	^c CASING	ic Water Le	evel			Та	Potability	Sub Sround Level h to water level Elapsed Time Minutes:Sec 1:00 2:00 3:00 4:00 5:00 7:00 8:00 10:00 14:00 20:00 30:00 40:00 60:00	Rec	ement in Imp tovery (ft) 189.00 177.00 174.50 173.50 173.55 172.58 172.58 172.33 171.83 171.42 170.00 169.75 169.42 169.17

Contractor Certification Name of Journeyman responsible for drilling/construction of well UNKNOWN NA DRILLER Company Name TALL PINE DRILLING LTD.

Certification No 1

Copy of Well report provided to owner Date approval holder signed

Printed on 9/7/2021 12:49:46 PM

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Part 2 - Technical Requirements

Application under the Agricultural Operation Practices Act for a confined feeding operation, manure collection area, and/or manure storage facility(ies)

GENERAL ENVIRONMENTAL INFORMATION

(complete this section for the worst case of the existing facility which is the closest to water bodies or water wells and for each of the proposed facilities) Facility description / name (as indicated on site plan) Proposed 1: Feedlot pens

Existing:

Proposed 2: Catch basin

Proposed 3:

Topose	d 2:			Flopose	u 3:			
Eacili	ity and environmental risk	Facilities				NRCB USE ONLY		
Facili	information	Existing	ting Proposed 1	Proposed 2	Proposed 3	Meets requirements	Comments	
Flood plain information	What is the elevation of the floor of the lowest manure storage or collection facility above the 1:25 year flood plain or the highest known flood level?	☑ >1 m □ ≤1 m	Ø >1 m □ ≤ 1 m	Ø >1 m □ ≤ 1 m	□ > 1 m □ ≤ 1 m	YES INO YES with exemption	not in known flood plain	
	How many springs are within 100 m of the manure storage facility or manure collection area?	0	0	0		YES NO	none observed or reported	
Surface water information	How many water wells are within 100 m of the manure storage facility or manure collection area?	0	0	0		YES NO	one within 100 m of pens, see TD page 6	
Sur	What is the shortest distance from the manure collection or storage facility to a surface water body? (e.g., lake, creek, slough, seasonal)	2630m	2630m	2630m		YES NO	> 500 m to intermittent creeks	
water ation	What is the depth to the water table?		2.59m	2.59m		YES NO	see Decision Summar RA21043	
Groundwater information	What is the depth to the groundwater resource/aquifer you draw water from?	64m	64m	64m		YES NO YES with exemption	15.2 m based on AEP water wells 93973 and	

Additional information (attach supporting information, e.g. borehole logs, records, etc. you consider relevant to your application)

Last updated February 26, 2021

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NRCB USE ONLY ENVIRONMENTAL RISK SCREENING INFORMATION

$\ensuremath{\mathsf{ERST}}$ for $\ensuremath{\underline{\mathsf{proposed}}}$ facilities

Facility	Groundwater score	Surface water score	File number
Pens	Low	Low	RA21043
Catch basin	Low	Low	RA21043

ERST for existing facilities

Facility	Groundwater score	Surface water score	File number
As noted on page 2 the remains		not be used to collec	t or store manure, for this
reason I did not risk screen th	ns lacinty.		

ERST related comments:



NRCB USE ONLY WATER WELL AND SURFACE WATER INFORMATION								
	WAILIDS: 286659 and 288714							
Well IDs:	200009 and 200	0/ 14	·					
Surface water rel	ated concerns from di	rectly affected parties or refe	erral agencies:		🗙 yes 🗖 No			
		ectly affected parties or refe	-					
Water wells	□ N/A							
		ance requirements applied:		required:	🗆 yes 본 no			
Surface water	X N/A							
If applicable, exe	mption for 30 m dista	nce requirements applied:	YES NO Condition	required:				
Water Well Exe	mption Screening To	DOI 🗌 N/A						
Wate	er Well ID	Preliminary Screening	Secondary Screening		Facility			
		Score	Score					
286659		35 (continue)	7 (exemption mo	re likely)	Pens			
Groundwater or	r surface water relat	ted comments:						





Part 2 – Technical Requirements

Application under the Agricultural Operation Practices Act for a confined feeding operation, manure collection area, and/or manure storage facility(ies)

DISTANCE OF ANY MANURE STORAGE FACILITY (EXISTING OR PROPOSED) TO NEIGHBOURING RESIDENCES

			NRCB USE ONLY				
Neighbour name(s)	Legal land description	Distance (m)	Zoning (LUB) category	category	Distance (m)	Waiver attached (if required)	Meets regulations
Curtis and Lorraine Tonneson	05-14-42-25 W4	1058	CRH	1	1,045	n/a	yes
Klaus Van Der Molen	04-22-42-25 W4	1047	CRH	1	1,030	n/a	yes
Don and Monica Brennan	12-14-42-25 W4	665	Α	1	670	n/a	yes
Brad and Sarah Overreem	02-15-42-25 W4	1160	Α	1	1,200	n/a	yes
Sipke and Margriet Dijkstra	15-22-42-25 W4	1370	Α	1	1,280	n/a	yes

LAND BASE FOR MANURE AND COMPOST APPLICATION (complete only if an increase in livestock or manure production will occur)

				NRCB	USE ONLY
Name of land owner(s)*	Legal land description	Usable area** (ha)	Soil zone ***	Usable area (ha)	Agreement attached (if required)
Double T	section 15-42-25 w4	242.8	Black	198	
Double T	sw-14-42-25 w4	56.7	Black	50	
Morsan	north 20-42-25 w4	93.1	Black	81	yes
	SE 25-42-25 W4	140ac/57 ha		45	ves
	SE 12-43-25 W4	109 ac/44 ha	a Total	41	yes

* If you are **not** the registered landowner, you must attach copies of land use agreements signed by all landowners.

** Available manure spreading area (excluding setback areas from residences, common bodies of water, water wells, etc. as identified in Agdex 096-5 Manure Spreading Regulations)

*** Brown, dark brown, black, grey wooded, or irrigated

Additional information (attach any additional information as required)

Last updated February 26, 2021

Ponoka County's Land use bylaw zones and the applicable MDS categories are discussed in Decision Summary RA21043.

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NRCB USE ONLY			
MINIMUM DISTANC			
Methods used to determine	distance (if applicable)	scaled air ph	oto, 2021 from Google Earth
Margin of error (if applicabl			
Requirements (m): Categor	ry 1: (Category 2: 878	Category 3: 1,098 Category 4: 1,756
Technology factor:			🗆 YES 🖾 NO
Expansion factor:			YES 🕅 NO
MDS related concerns from The MDS related cor		-	es: Ž YES П NO I Summary RA21043.
LAND BASE FOR MA		OST APPLICA	TION
Land base required:	351 ha (black)	-	
Land base listed:	493.6 ha	-	
Area not suitable:	78.6 ha	-	
Available area	415 ha	-	Requirement met: 🖄 YES 🗖 NO
Land spreading agreements	s required: 🛛 🗴 YE	s 🗆 no	
Manure management plan:	T YE	s 🖄 NO	If yes, plan is attached:
PLANS			
Submitted and attached con	nstruction plans:	🎽 yes 🗖 no	
Submitted aerial photos:		본 yes 🗌 no	
Submitted photos:		🗆 yes 🛛 no	
GRANDFATHERING			
Already completed: If already completed, see _	Decision Summar	⊠ yes □ no <u>y RA02</u> 053	□ N/A

NRCB received May 12, 2022

Manure Spreading Agreement

This agreement is between	Double T Cattle	, manure
producer, and		

____Morsan Farms_______Manure receiver.

Length of agreement: This agreement is valid for a time period of _____3 years_____(minimum of three years)

Legal land location	Soil type ¹	Acres suitable spreading ²	
N 20-42-25-W4	Black	230 acres	81 ha available
SE-25-42-25-W4	Black	140 acres	45 ha available
SE-25-42-25-W4	Black	109 acres	<u>41 ha availab</u> l

¹ Soil type choices: Dark brown and brown, Grey wooded, Black, Irrigated.

² Land within required setbacks from water bodies, water wells, residences, etc. is not to be included.

Other comments:

Manure producer (confined Feeding Operation) Legal Land Location_____

May 12 2022 Date of signing

Signature

See Thales.

Print name

Corporate name(if appl)

Manure Receiver – Landowner(s)³

May 12 2022 Date of signing

Har Moins Thaten.

Signatu

Print name

Corporate name(if appl)

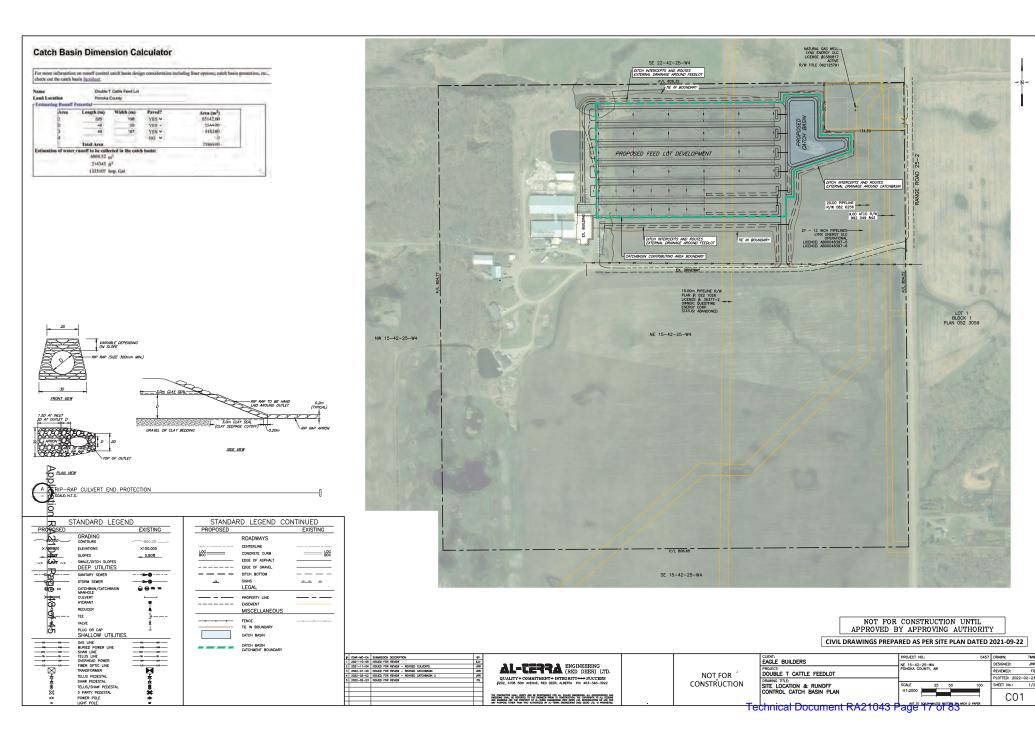
Date of signing

Signature

Print name

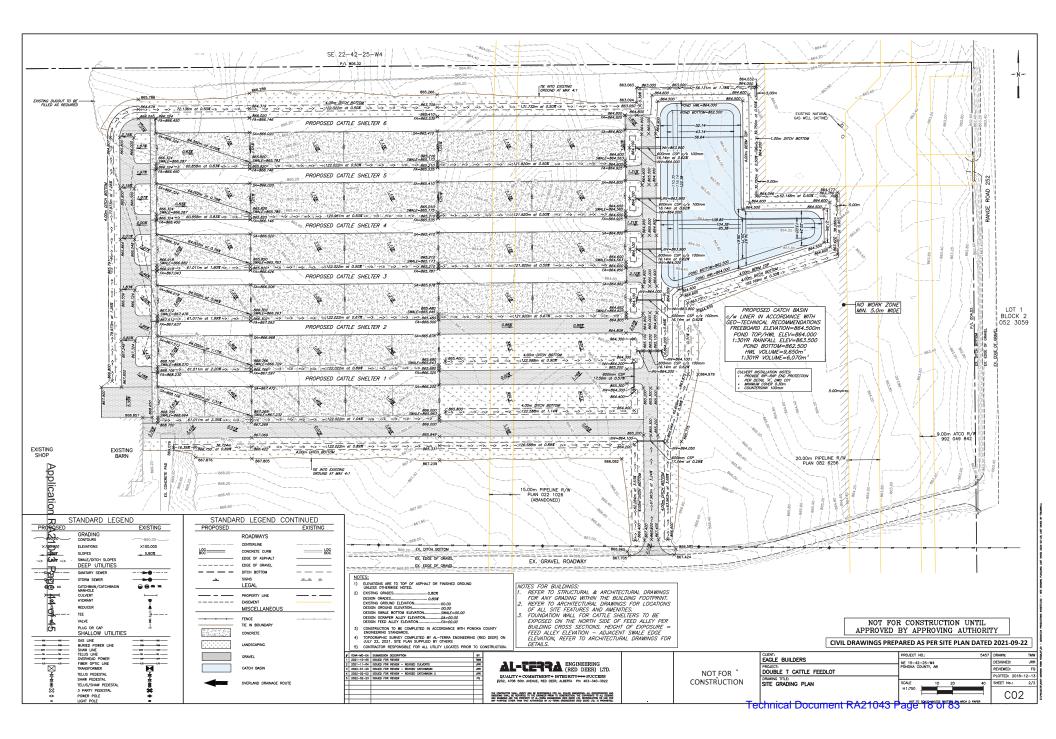
Corporate name(if appl)

³ All registered owners of land, or authorized signing authorities must sign.



Ń-

JRR





Layfield's HDPE geomembranes are manufactured to meet GRI-GM13 Standard Specification and have been extensively used in a variety of containment applications. HDPE geomembranes have low permeability, good ultra violet resistance, and excellent chemical resistance. HDPE 60 geomembrane is a field assembled lining material that must be installed by trained installers. HDPE is used in a multitude of applications such as a landfill liner, a pond liner, and in water containment projects.

Property	nembrane Properties Test Method	Values	Testing Frequency
Thickness (min. avg)	ASTM D5994	1.50 mm	
Thickness, lowest individual for 8 out of 10 values		1.53 mm	Every Roll
Sheet Density (min.)	ASTM D792	0.940 g/cc	Every 90,000 kg
Tensile Properties (min. avg.)			
Break Strength		40 kN/m	
Break Elongation (calculated at gage length of 2 in.)	ASTM D6693	700%	Every 9,000 kg
Yield Strength	Type IV	22 kN/m	
Yield Elongation (calculated at gage length of 1.3 in.)		12%	
Tear Resistance (min. avg)	ASTM D1004	187 N	Every 20,000 kg
Puncture Resistance (min. avg)	ASTM D4833	480 N	Every 20,000 kg
Stress Crack Resistance (min.)	ASTM D5397	500 hrs	Once every two resin
	(Appendix X1)		railcars
High Pressure Oxidative Induction Time (min.)	ASTM D5885	400 minutes	Every 90,000 kg
Carbon Black Content	ASTM D4218	2.0 - 3.0%	Every 9,000 kg
Carbon Black Dispersion	ASTM D5596	9 out of 10 in CAT 1	Every 20,000 kg
		or 2; 1 in CAT 3	
Oven Ageing at 85° C	ASTM D5721		
% retained HPOIT after 90 days (min.)	ASTM D5885	80%	Once per formulation
UV Resistance	ASTM D7238		
% retained HPOIT after 1600 hrs (min.)	ASTM D5885	50%	Once per formulation

Resin Properties						
Resin Density (minimum)	ASTM D792	0.932 g/cc	Once per railcar			
Resin Melt Index at 2.16 Kg/190°C (max.)	ASTM D1238	1.0 g/10 min	Once per railcar			

Thermally Bonded Seam Strength (as per GRI-GM19)					
ASTM D6392	525 N/25mm	Not Applicable			
ASTM D6392	398 N/25mm	Not Applicable			
ASTM D6392	525 N/25mm	Not Applicable			
ASTM D6392	340 N/25mm	Not Applicable			
	ASTM D6392 ASTM D6392 ASTM D6392	ASTM D6392 525 N/25mm ASTM D6392 398 N/25mm ASTM D6392 525 N/25mm			

Typical Roll Dimensions (Rolls dimensions may vary ± 1%)			
Roll Width	6.86 meters		
Roll Length	158.5 meters		

Latest product specifications are available on Layfield Group website <u>www.layfieldgroup.com</u>

Disclaimer: Layfield disclaims any and all express, implied, or statutory standards, warranties or guarantees, including without limitation any implied warranty as to merchantability or fitness for a particular purpose or arising from a course of dealing or usage of trade as to any equipment, materials, or information furnished herewith. This document should not be construed as engineering advice.



Part 2 – Technical Requirements

Application under the Agricultural Operation Practices Act for a confined feeding operation, manure collection area and/or manure storage facility(ies)

LIQUID MANURE STORAGE: Synthetic liner

(complete a copy of this section for EACH proposed liquid manure storage facility with a synthetic liner)

Facility description / name (as indicated on site plan)

1. Feedlot Catch Basin

Manure storage capacity (use one row in the table for EACH cell of the synthetic lined storage, attach additional pages if you require more rows)

2.

			1.1.1			Slope run:rise		NRCB USE ONLY	E ONLY
	Length (m)	Width (m)	Total depth (m)	Depth below ground level (m)	Inside end walls	Inside side walls	Outside walls	Calculated storage capacity (excl. 0.5 m freeboard) (m ³)	Filled in lower ¼? Y/N
1.	-95-	110.	2	+1.5*	3:1	3:1	4:1	9,650	no
2.	Sec	Drawn	satta	hed for St	400 1	and			
		Volue	-	56.64× 122. 38-61×52		TOTA	AL CAPACITY		

Surface water control systems

Describe the run-on and runoff control system

Berms elevated above surrounding landscape with 0.5m free-board.

* the southwest corner will be approximately 2.1 m below ground, the water table was observed to be as shallow as 2.47 m below ground surface in fall 2021. A condition will be added to the permit, see discussion in Decision Summary RA21043.

Sealing

Describe sealing practices for piping, etc. that penetrates the	ie liner
Pipe boot welded to liner and clamped to pipe.	
	Requirements met: X YES NO
iner protection	
Describe how the inside walls, bottom and outside walls are	protected from erosion
Concrete pad will be poured under pipe fill area. Veget	tation on exterior berm slope.
Describe how the physical integrity of the liner will be maint	tained from other damage
Care and caution will be used to prevent damage to line	er.
	Requirements met: 🖄 YES 🗖 NO

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Part 2 – Technical Requirements



Application under the Agricultural Operation Practices Act for a confined feeding operation, manure collection area and/or manure storage facility(ies)

LIQUID MANURE STORAGE: Synthetic liner (cont.)

Synthetic liner details

Provide synthetic liner material details 60mil HD liner. Spec sheet attached.

Additional information (attach copies of design/engineering reports)	NRCB USE ONLY		
	Requirements met:	X YES D NO	
	Condition required:	X YES D NO	
	Report attached:	VES X NO	

As noted previously, a condition will be a	Require Require Require	ements met: ements met: address wate	☐ YES ⊠ NO ⊠ YES ☐ NO er table separation.
ERST completed: 🛛 see ERST page for details			
Surface water control systems Requirements met: X YES NO	Details/comments:		
Synthetic liner requirements Leakage detection system required:	🗆 yes 🖾 no	If yes, please	explain why.
Construction plans approved by professional engineer: Will liner be installed by manufacturer approved contract Preparation of liner bed (comments): A condition will be added requiring the line that a completion report be submitted.		☐ YES ☑ NO ☑ YES ☐ NO qualified thi	D
Condition required: X YES NO			





NRCB USE ONLY						
RUNOFF CONTROL CATCH BASIN CAPACITY SUMMARY (if applicable)						
Facility 1 feedlot						
Name / description catch basin	Capacity 9,650 m ^{3*}					
Facility 2						
Name / description	Capacity					
Facility 3						
Name / description	Capacity					
Facility 4						
Name / description	Capacity					
TOTAL CAPACITY	9,650 m ³					
RUNOFF VOLUME FROM CONTRIBUTING AREAS	5,901 m ³					
MEETS AOPA RUNOFF CONTROL VOLUME REQUIREMENTS	XYES NO					

* the stated catch basin capacity is reasonable, see page 76 below.

The approximate catchment area for the catch basin is 81,600 m². Of this, approximately 62,000m² will be either paved by concrete, covered by roofs, or have a synthetic liner.

The 1:30 year rainfall event in the the Standards and Administration regulation for Ponoka is 80 mm.

 $62,000m^2 \times 0.080 \text{ m} \times 1.0 \text{ (runoff coefficient for "paved" area)} = 4,960 \text{ m}^3$ 19,600 m² x 0.080 m x 0.6 (runoff coefficient for unpaved area with 80 mm rainfall) = 941 m³

Based on the above, I would expect there to be approximately 5,901 m³ of runoff directed to the catch basin in a 1:30 year rainfall event.

Part 2 — Technical Requirements



Application under the Agricultural Operation Practices Act for a confined feeding operation, manure collection area and/or manure storage facility(ies)

SOLID MANURE, COMPOST, & COMPOSTING MATERIALS: Barns, feedlots, & storage facilities -Concrete liner

(complete a copy of this section for **EACH** barn, feedlot, and storage facility for solid manure, composting materials, or compost with a concrete liner)

Facility description / name (as indicated on site plan)

1. Feedlot pens

2._

Manure storage capacity

	Length (m)	Width (m)	Depth below grade to the bottom of the liner (m)	NRCB USE ONLY Estimated storage capacity (m ³)
1.	4 x 304.8	32.97	0	
2.	2 x 182.88	32.97	0	
			TOTAL CAPACITY	

☑ I plan to use a short-term solid manure storage (STMS) as part of my manure storage and handling plan for this CFO. The AOPA requirements for STMS are set out in the NRCB <u>Short-Term Solid Manure Storage Requirements Fact Sheet</u>.

Surface water control systems

Describe the run-on and runoff control system Catch basin used

Liner protection

Describe how the physical integrity of the liner will be maintained Cleaned and inspected periodically

NRCB USE ONLY

Requirements met: 🖄 YES 🗋 NO

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Part 2 – Technical Requirements

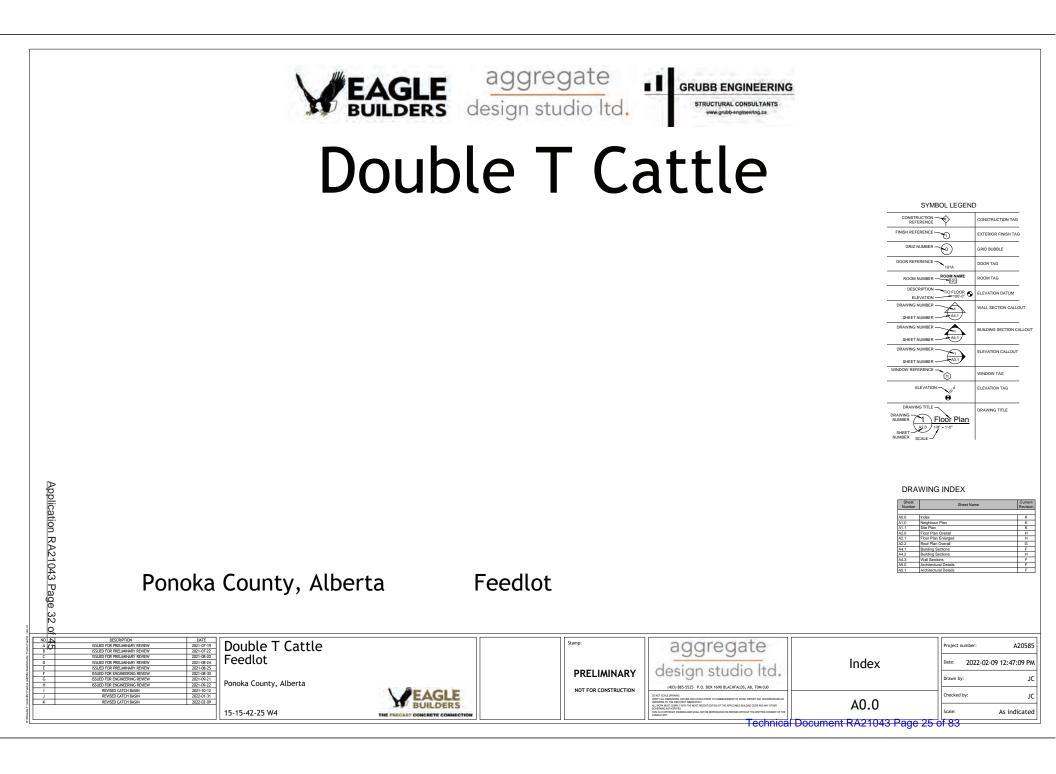


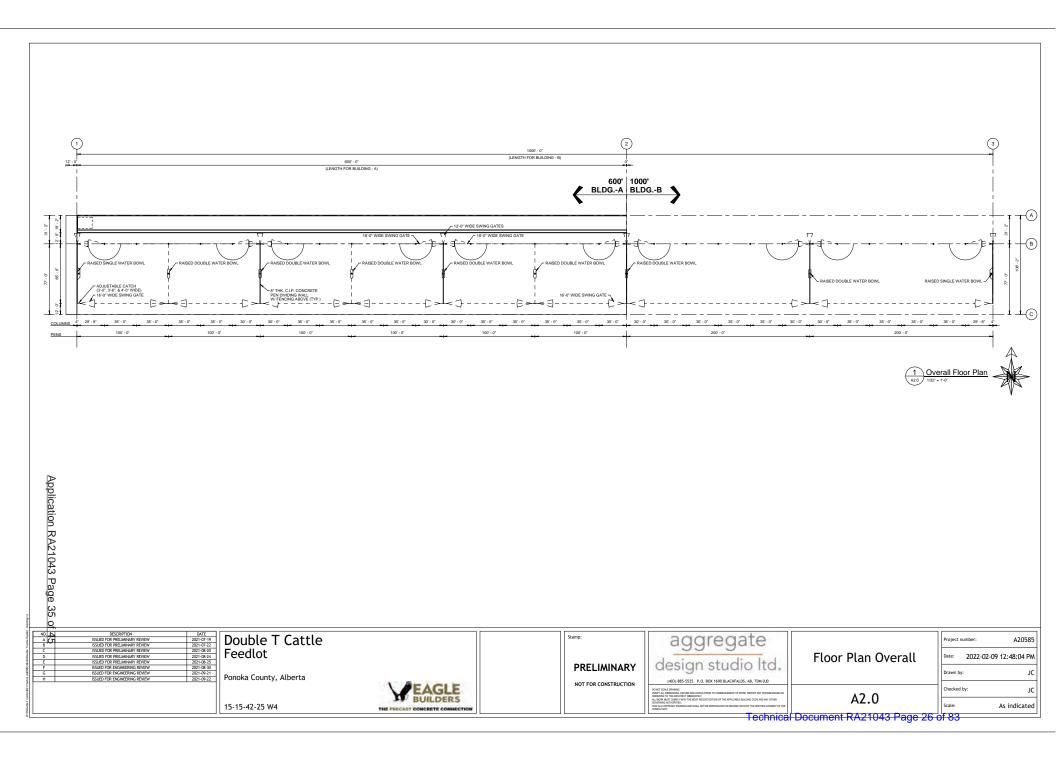
Application under the Agricultural Operation Practices Act for a confined feeding operation, manure collection area and/or manure storage facility(ies)

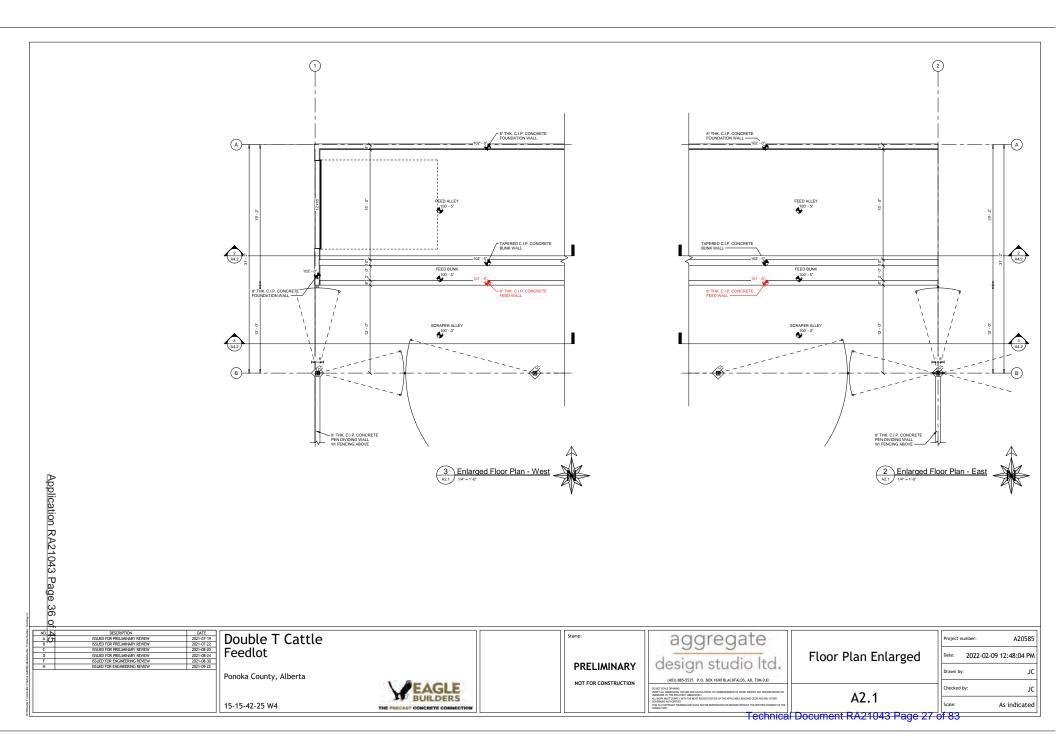
SOLID MANURE, COMPOST, & COMPOSTING MATERIALS: Barns, feedlots, & storage facilities -Concrete liner (cont.)

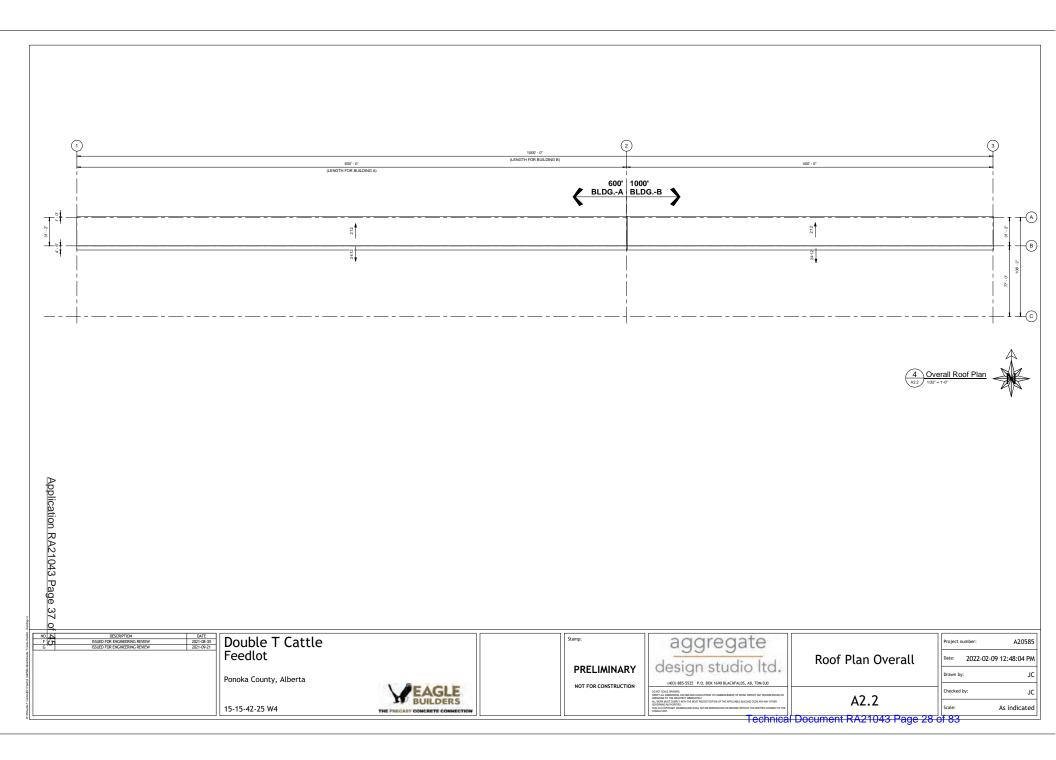
Concrete liner details					
Concrete thickness		Method of su	phate protection:		
0.152m (6")		type 10 HS cement			
Concrete strength		Concrete reinforcement size and spacing			
30 mpa		10M bar at 0	.305m on center e	ach way	
Concrete requirements car Guideline minimums: Solid manure: 25MPa (D) Solid manure (wet): 30MPa (C Method of sulphate protection Type 50 or Type 10 with fly a: Additional information (a	ı: sh or equivalent	Agdex 096-93		nents met: n required:	YES INO
NRCB USE ONLY				-	
Nine month manure stora	ge volume requirements met 🛛	YES 🛛	YES With STMS		
Depth to water table:	2.47 m	Red	quirements met:	K YES	NO
Depth to Uppermost grou	ndwater resource: 15.2 m	Ree	quirements met:	K YES	NO
ERST completed: 🚺 see	ERST page for details				
Surface water control s Requirements met: 🔽 YE					
Concrete liner details					
large concrete pac permit requiring 1. proposed and 2. th	crete and rebar meet the ds can be prone to crack the pad be constructed ne pad/pens to have ade required: YES 🛛 NO If y	king. Accord with an eque equate seale	ingly, condition uivalent concreted ad expansion jo	s will be a te liner with	dded to the n rebar as

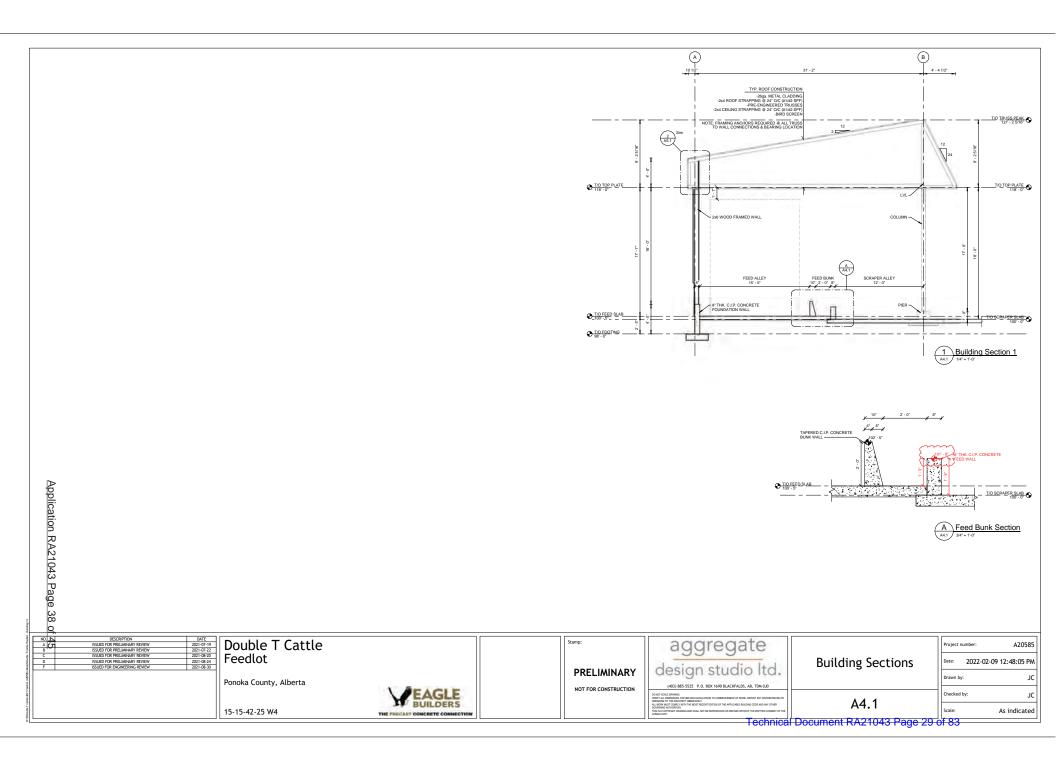
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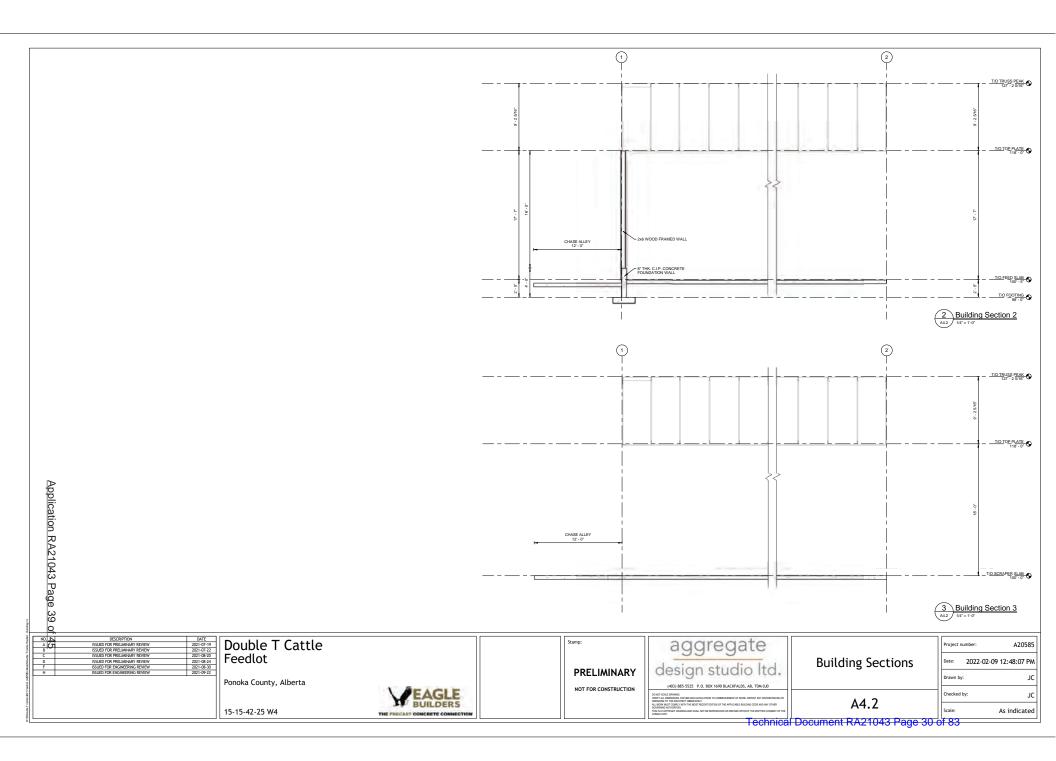


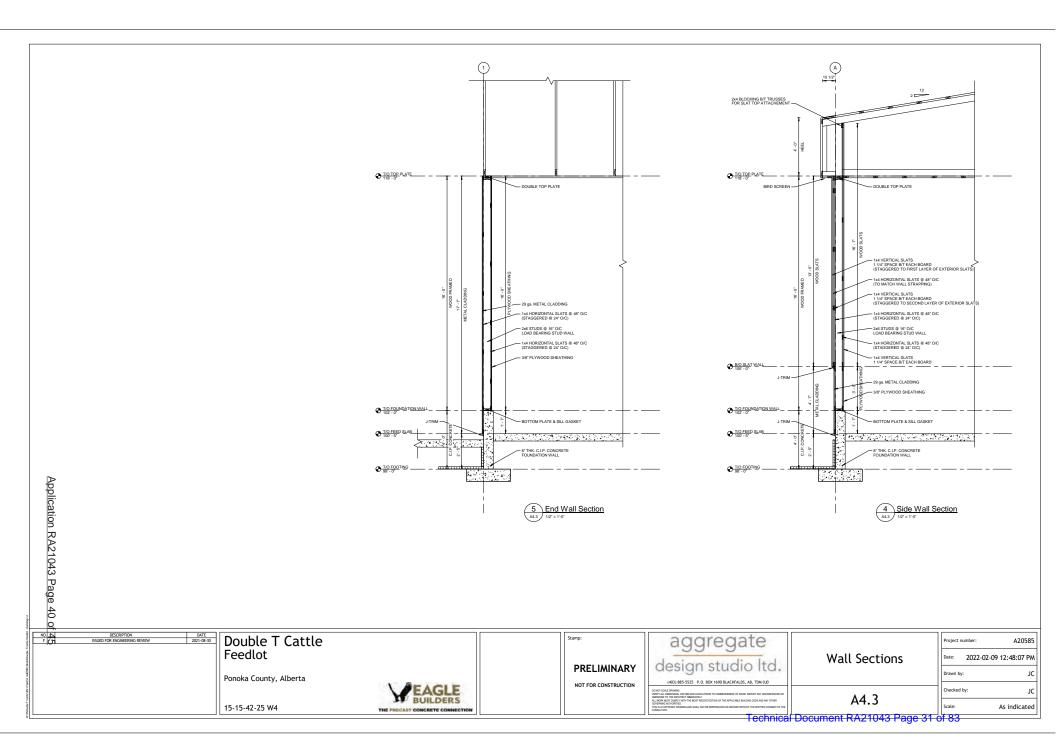


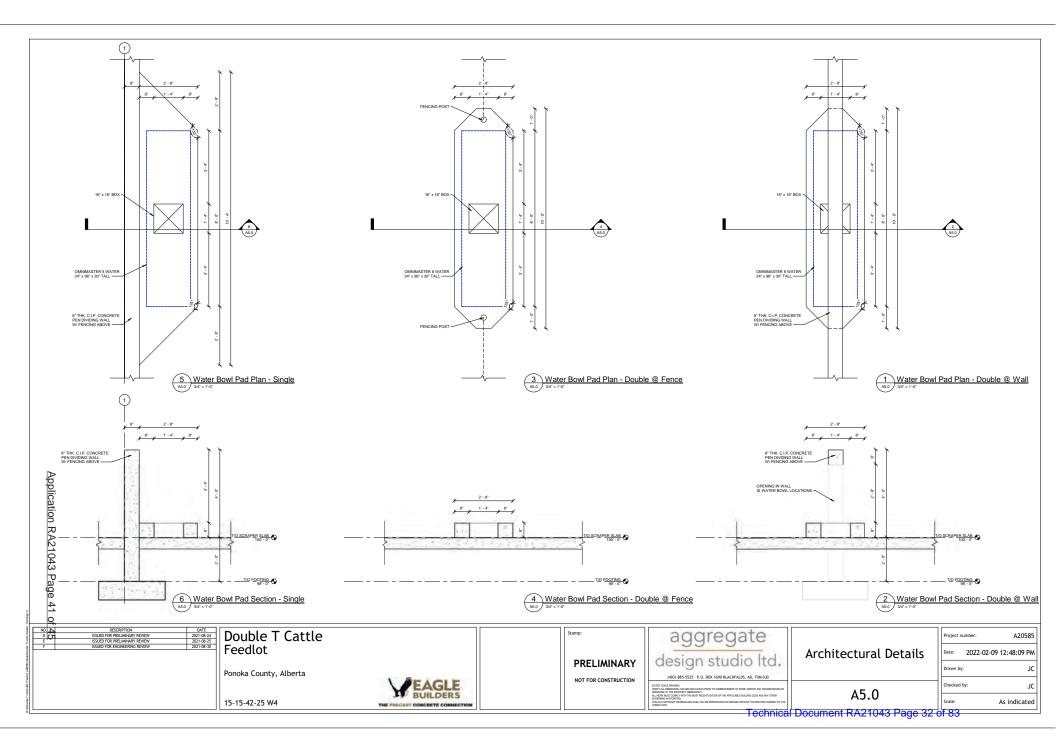


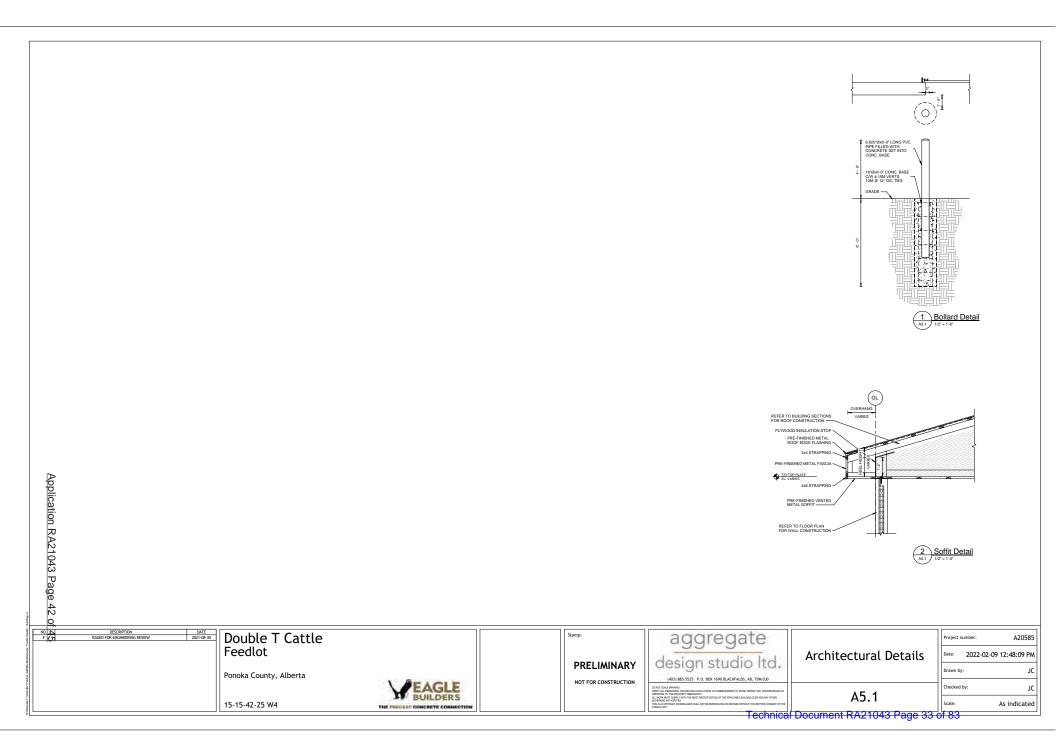












Union Street Geotechnical

7th October, 2021 File No. USG1276

Eagle Builders LP 27312 - 17 Twp. Rd. 394 Aspelund Industrial Park Blackfalds, Alberta T0M 0J0

ATTENTION: Mr. Allan Prediger, Project Manager

Dear Mr. Prediger,

SUBJECT: Double T Cattle Co. Proposed Confined Feedlot N.W. ¼ of 15-42-25 W4M Ponoka County, Alberta

1 INTRODUCTION

Union Street Geotechnical Ltd. (Union Street) was retained by Eagle Builders LP (Eagle Builders) to perform a field investigation, and subsequent laboratory testing on the subgrade, to aid in the design and construction of a proposed confined feedlot for Double T Cattle Co. located within the N.W. ¼ of 15-42-25 W4 in Ponoka County, Alberta, as shown on Drawing No. A1. Nine boreholes were advanced in the proposed pen and catch basin development footprint for liner design purposes. Based on the boreholes advanced, it was determined that the upper subgrade is predominantly composed of till overlying mudstone.

2 DESCRIPTION OF THE PROJECT AND SITE

2.1 SITE DESCRIPTION

The site is located approximately 1.5 km north-northwest of the intersection of Range Road 252 and Township Road 422, within the N.W. ¹/₄ of 15-42-25 W4 in

4726 - 78A Street Close Red Deer, Alberta T4P 2J2

Bus: 403-350-9688 www.unionstreetgeo.ca Ponoka County, Alberta, as shown on Drawing No. A1. The proposed feedlot development site within the N.W. ¹/₄ was relatively flat with the geological drainage of the area sloping east.

The proposed feedlot is currently utilized as agricultural land and bordered by agricultural land to the north, east, south, with the existing agricultural development to the west-southwest of the proposed feedlot. Photographs depicting the site are attached to this report.

2.2 PROPOSED DEVELOPMENT

The proposed development consists of feedlot pens, catch basin, and associated development. Specific development details are unknown at the time of this report writing but are assumed to be typical to those in the area and for developments of this nature.

Recommendations contained in this report have been given for the above described development and those typical of a development of this nature. If there are any changes to the proposed development, or their locations, these changes should be reviewed by Union Street personnel to confirm the applicability of this report to the revised development plans.

3 FIELD INVESTIGATION AND LABORATORY ANALYSIS

The field investigation program included drilling nine boreholes at the locations shown on Drawing No. A2. The borehole locations were established by Union Street personnel based on a discussion with the owner, proposed development footprint, utility clearance, and access. No formal surveying of the borehole locations or site were completed and therefore, all drawings, locations, measurements, and legal descriptions are approximate and conceptual in nature.

On 14th September, 2021, nine boreholes (designated as BH101 to BH109) were advanced using a truck-mounted auger drill utilizing 150 mm diameter, continuous flight augers, operated by Venom Environmental Drilling Ltd. The boreholes were advanced to a depth of 4.57 m to 9.14 m below ground surface.



3.1 GENERAL STRATIGRAPHY

The subsurface conditions were relatively uniform in all nine borehole locations for liner design purposes. In general, and to the depths drilled, the soil conditions encountered at the borehole locations generally consisted of, in descending order; topsoil overlying till and mudstone. Topsoil, with an approximate average thickness of 320 mm, was encountered at surface in all nine boreholes. Till, with varying clay, silt, and sand content was encountered underlying the topsoil in all nine boreholes which extended to an average depth of 3.13 m below grade. It was yellowish brown (10YR 5/8) to dark grey (10YR 4/1), oxidized to non-oxidized, moist, soft to hard, massive, contained gravel, silt pocket, and coal chip inclusions, and was calcareous. A thin sand seam was encountered within the till in Borehole BH106. Mudstone was encountered underlying the till in all nine boreholes which extended to the maximum exploration depth. The mudstone generally consisted of clayey silt with trace to some sand. Observations made during the field investigation, visual descriptions of the soils, and the results of laboratory analysis are presented in the attached Borehole Logs and Laboratory Test Results.

Undisturbed samples were collected within the till encountered in Borehole BH102 to aid in the proposed catch basin liner design and within the till encountered in Borehole BH109 to aid in the proposed pen liner design. Sample MW16, obtained from Borehole BH102 at 4.57 m below grade, was submitted for hydraulic conductivity testing which indicated a permeability value of 7.87×10^{-9} cm/s. Sample MW48, obtained from Borehole BH109 at 3.05 m below grade, was submitted for hydraulic for hydraulic conductivity testing which indicated a permeability value of 6.61×10^{-7} cm/s.

Three MUSC tests were performed on till samples obtained from Boreholes BH101, BH105, and BH107. The MUSC results are summarized in Table 3.1.



Sample No. and Depth	Borehole No.	Liquid Limit (%)	Plastic Limit (%)	Plasticity Index (%)	Moisture Content (%)	MUSC – Soil Type
MW3 - 2.29 m	BH101	51.9	11.8	40.1	16.5	СН
MW29 - 0.76 m	BH105	52.4	11.3	41.1	11.4	СН
MW35 - 0.76 m	BH107	40.1	13.0	27.1	12.2	CI
Average	:	48.1	12.0	36.1	13.4	CI-CH

TABLE 3.1: SUMMARY OF TILL MODIFIED UNIFIED SOILS CLASSIFICATION TEST RESULTS

Based on the results in Table 3.1 the till has an average MUSC of "CI-CH" - Silts or Clays of medium to high plasticity.

Four Mechanical Wash Sieves (MWSs) were performed on till samples obtained from Borehole BH101, BH105, BH107, and BH109. The MWS sieve results are summarized in Table 3.2.

Sample No. and Depth	Borehole No.	Gravel Content (%)	Sand Content (%)	Silt Content (%)	Clay Content (%)
MW3 - 2.29 m	BH101	0.4	33.2	66	5.4
MW29 - 0.76 m	BH105	1.9	31.5	66	5.6
MW35 - 0.76 m	BH107	0.6	33.5	65	5.8
MW45 - 0.76 m	BH109	0.1	67.5	32	2.4
Average:		0.8	41.4	57	.8

TABLE 3.2: SUMMARY OF TILL MUSC AND PSA TEST RESULTS

Cobbles and boulders were not encountered during drilling, but as till is a heterogeneous mixture of all grain sizes, cobbles and boulders may be encountered during construction.

A Particle Size Analysis (PSA) and MWS were performed on mudstone samples obtained from Borehole BH101. The PSA and MWS results are summarized in Table 3.3.



Sample No. and Depth			Sand Content (%)	Silt Content (%)	Clay Content (%)
MW5 - 3.81 m	BH101	0.0	17.7	82	2.3
MW7 - 5.33 m	BH101	0.0	0.9	67.9	31.2
Average:		0.0	9.3	54.5	36.2

TABLE 3.3: SUMMARY OF MUDSTONE SIEVE AND HYDROMETER TEST RESULTS

Notes:

1 - The fines results of MW5 were split 50/50 in the average.

3.2 GROUNDWATER

Seepage was observed in Boreholes BH101 to BH103 at an average depth of 6.71 m below grade and three piezometers were installed following drilling. The groundwater elevation was recorded on the 28th September, 2021, 14 days following drilling, and the results are summarized in Table 3.4.

Borehole No.	Borehole Depth (m)	Groundwater Level ¹ (m), 28 th September, 2021
BH101	7.93	2.47
BH108	9.14	2.68
BH109	4.57	2.63
Average:		2.59

TABLE 3.4: SUMMARY OF GROUNDWATER MEASUREMENTS

Notes:

1 - Below existing grade.

Based on seepage encountered during drilling and the groundwater elevations recorded in the piezometers, the average groundwater table is likely (approx.) 2.0 m to 3.0 m below ground surface. Groundwater levels are subject to meteorological events, seasonal variations, site gradient, and other salient factors resulting in the water table varying with time.



4 **REFERENCES**

The following was referenced while composing this letter:

- Province of Alberta, "Agricultural Operation Practices Act and Regulations", Revised Statutes of Alberta 2000, Chapter A-7, Alberta Queen's Printer, 2010;
- Province of Alberta, "Agricultural Operation Practices Act and Regulations", Standards and Administration Regulation, Part 2, Alberta Queen's Printer, 2017;
- Alberta Government, "Catch Basin Design and Management", Technical Guideline Agdex 096-101, August 2012;
- Natural Resources Conservation Board, "Determining Equivalent Protective Layers and Constructed Liners", Technical Guideline Agdex 096-61, May 2013; and,
- AL-Terra Engineering (Red Deer) Ltd., "Site Location & Runoff Control Catch Basin Plan", Project No. 5457, dated 6th October, 2021.

5 FEEDLOT PENS

5.1 STRIPPING

All organic soil, vegetation, sand, etc. should be stripped from the feedlot footprint prior to the start of feedlot grading construction activities.

5.2 NATURALLY OCCURRING LINER

The Natural Resources Conservation Board (NRCB) requires naturally occurring protective layers for solid manure collection and storage facilities, such as feedlots, to have a minimum thickness of 2.0 m and a maximum hydraulic conductivity of 1.0×10^{-6} cm/s. Based on the average thickness of the till stratum encountered in the six boreholes advanced in/near the proposed feedlot footprint, 2.79 m, and the



factored hydraulic conductivity test result of the till in Borehole BH109, 6.61x10⁻⁶ cm/s, the encountered native till in the vicinity of Borehole BH109 does not meet the naturally occurring protective layer requirement.

5.3 COMPACTED SOIL LINER

The NRCB requires compacted soil liners for solid manure collection and storage facilities, such as feedlot pens, to have a minimum thickness of 0.5 m and a maximum hydraulic conductivity of 5.0×10^{-7} cm/s. A hydraulic conductivity analysis was performed on a native till sample obtained from Borehole BH102 at 4.57 m below grade and which had a factored result of 7.87×10^{-8} cm/s. Native till utilized as fill obtained from the vicinity of Borehole BH102 (eastern portion of the site) compacted to a minimum 1,902 kg/m³ dry density at 15.1% moisture will be suitable as a clay liner across the feedlot and meets NRCBs soil liner requirement.

If a compacted soil liner is utilized, the NRCB requires the bottom of the soil liner to be equal aor greater than 1.0 m from the groundwater table at the time of construction.

5.4 CONCRETE LINER

The client has indicated that the pens will likely utilize a concrete liner. If concrete is utilized, it must offer the equivalent protection of a 0.50 m thick soil liner with a permeability of not more than 5.0×10^{-7} cm/s. The type of concrete proposed for the liner is unknown at this time, but is expected to well exceed this requirement.

5.5 GRADING

The base of the pens must be positively graded, to ensure liquids don't pond on the subgrade, to a catch basin or other runoff control system. It is assumed that till, from cut/fill grading activities, will be utilized during construction if fill is required. Due to its plasticity, the till isn't recommended for areas requiring structural fill.

Fill, composed of native till, should be placed in lifts not exceeding 200 mm and compacted to a minimum 98% of its Standard Proctor Dry Density (SPDD) at moisture contents +2% of optimum. The local soils may require moisture



conditioning to achieve the required degrees of compaction. The degree to which moisture conditioning of the fill would be required may vary with the local soils and construction season. There may also be some localized areas where the native soils may require drying, or blending with drier soils, in order to achieve the required degrees of compaction.

6 CATCH BASIN

6.1 CAPACITY

For preliminary design purposes, the design volume of the catch basin must have a storage capacity that can accommodate a 1 in 30 year rainfall. For the Ponoka region a 1 in 30 year event equates to approximately 80 mm of rainfall. The drainage area of the feedlot, including the proposed catch basin, is approximately 79,703 m². The following was utilized to determine the catch basins miniumu required capacity.

$$V_{30} = D_A \times R_{30} \times C_R$$

Where:

 V_{30} = One Day Rainfall Volume (m³); D_A = Drainage Area (m²); R_{30} = One Day Rainfall (m); and, C_R = Runoff Coefficient (1.0 for a paved area).

Based on the referenced formula, it has been determined that the expected one day rainfall volume for the site is approximately 6,376.2 m³. However, to ensure the liners integrity due to drying out and cracking, and to increase the timeframe between emptying, the design capacity of the catch basin should be greater than the 1 in 30 year rainfall volume. Union Street recommends increasing the total volume capacity by approximately 60% of the 1 in 30 year rainfall minimum volume to approximately 10,137 m³.

The size and capacity of the catch basin may change depending on the liner option selected as, for example, a synthetic liner will allow a deeper catch basin, allowing a reduced footprint, reducing the required capacity. Therefore, although the general



footprint will remain similar, the size and location of the catch basin shown on the attached drawing may slightly differ from that actually constructed.

The catch basin must have a marker that is clearly visible at all times indicating the minimum volume required to accommodate a 1 in 30 year one day rainfall event.

6.2 STRIPPING

All organic soil and vegetation should be stripped from the catch basin footprint prior to the start of catch basin construction activities.

6.3 CATCH BASIN EXCAVATION

All till material from the catch basin excavation that is determined to be suitable for reuse should be stockpiled.

The banks of the catch basin should be cut at no steeper than 3H:1V. The capacity of the catch basin should designed ensuring a minimum 0.5 m freeboard. It is the responsibility of the contractor to remove water from trenches and excavations, regardless of origin. If while constructing the slopes of the catch basin subsurface, groundwater begins eroding the slopes and entering the catch basin, construction will need to be halted immediately and dewatering techniques will need to be implemented before construction continues. It is anticipated that potential groundwater problems can be resolved with well graded ditching and the installation of subgrade sumps around the perimeter of the site. If extreme groundwater seepage becomes present, more advanced dewatering techniques can be implemented. Although possible, it is not expected that seepage and sloughing will be encountered during construction unless excavations exceeds 2.6 m in depth.

Pumps and other materials necessary to keep the excavation free of water while work is in progress should be provided. Provisions should be made in case of accidental stoppage of dewatering equipment to prevent damage to the work area. The excavations must be protected against flooding and damage from surface run-off. Water removed from the site is to be disposed of in a manner that will not damage the work area or other property or persons.



Materials will be excavated and removed to the depths necessary for the construction of the structure and drainage system. Care must be taken to minimize the disturbance to the supporting soil. After the excavation has been shaped, any over-excavated areas will be backfilled and compacted to a density equal to or greater than the undisturbed soil. All slopes in the subgrade are to be uniform and in a condition suitable for a catch basin.

6.4 EMBANKMENTS AND FILL

An embankment/berm is recommended to be constructed around the perimeter of the feedlot to divert and minimize surface runoff from outside the operation from flowing into the catch basin. Additionally, a berm is recommended along the perimeter of the catch basin to prevent accidental effluent release outside of the operation and ensure a minimum 0.5 m freeboard. The exterior slope of a catch basin wall should be no steeper than 4H:1V. Any fills required can be constructed from the till subgrade encountered on-site. If an insufficient quantity of suitable on-site subgrade fill is not available, it will have to be analyses, imported, and compacted.

Areas requiring fills will be uniformly graded, scarified and re-compacted to the necessary density prior to being filled. Common excavated materials will be placed in the embankments, and in over-excavations if approved by the Geotechnical Engineer. Fills should be placed in lifts not exceeding 200 mm and compacted to minimum 98% of the SPDD at +2% Moisture. Fill material may require moisture conditioning prior to compaction.

6.5 LINER

6.5.1 Naturally Occurring Soil Liner

Following a review of the referenced NRCB documentation, it is understood that a naturally occurring protective layer for a catch basin must have a minimum thickness of 5.0 m and a maximum hydraulic conductivity of 1.0×10^{-6} cm/s. Additionally, the groundwater table must be approximately 1.0 m below the bottom of the naturally occurring liner. Laboratory testing was conducted on an undisturbed till sample in Borehole BH101 with a hydraulic conductivity of 7.87×10^{-9} cm/s. However, NRCB



requires laboratory permeability results to be reduced by an order of magnitude. When reduced by this magnitude, the design hydraulic conductivity of the till in the catch basin location is assumed to be 7.87×10^{-8} cm/s. Based on the average thickness of the till stratum encountered in Boreholes BH101 to BH103 and BH108 (boreholes advanced in/near the proposed catch basin footprint) and the factored hydraulic conductivity of the till, 2.80 m and 7.87×10^{-8} cm/s respectively. As such, a naturally occurring till layer 0.39 m thick with a permeability of 7.87×10^{-8} cm/s offers the equivalent protection of a 5.0 m thick layer with a permeability of 1.0×10^{-6} cm/s. A minimum liner thickness of 0.5 m is recommended however to ensure its structural integrity.

If a naturally occurring soil liner is utilized, the NRCB requires the bottom of the soil liner to be equal or greater than 1.0 m from the groundwater table at the time of construction.

6.5.2 Compacted Soil Liner

A compacted soil liner could be utilized at this site, but as the till's naturally occurring permeability meets the referenced requirements, it is unlikely that a compacted soil liner would be utilized at this site.

6.5.3 Geomembrane

If a catch basis with a great depth is required, to reduce the overall footprint, a synthetic liner can be used. If utilized, all geomembrane products should be handled, stored, and placed in accordance with the manufacturer's recommendations. Materials should be stored so that they do not come into contact with substances that may affect their physical or chemical properties such as fuel, exhausts, or petroleum products.

The installation contractor should be a contractor approved by the civil engineer who is trained to install the manufacturer's geomembrane. Installation should be performed by personnel experienced in seaming the materials under the constant supervision of the manufacturer. It is recommended that the installation contractor provide a written report on the completed installation certifying that the liner was



installed in accordance with the requirements of the manufacturer's specifications, the liner is ready for operation, and the warranty is in effect.

Geotextiles should be sufficiently anchored and deployed in a manner that will reduce folds and wrinkles. In the presence of wind, geotextiles should be weighted with sandbags or equivalent ballast. Geotextiles are to be cut using an approved cutter. Care should be taken in the installation process not to entrap excessive dust or stones that could damage the geomembrane.

The contactor should submit a panel layout proposal for the geomembrane to the engineer prior to the geomembrane placement. Care should be taken in the method used to unroll the panels so that damage to the liner or the supporting soil and/or geomembrane. Sand bags or equivalent ballast that will not damage the liner should be placed on the liner to prevent uplift. No equipment or tools that could damage the liner or underlying surfaces by handling or other means should be used. No personnel working on the liner will wear damaging shoes or engage in activities that could harm the liner, including smoking. All defects and damage will be documented and marked for repair. Repairs will be conducted in a manner suitable to the geomembrane manufacturer.

No NRCB technical specifications regarding synthetic liner were found. If utilized, it is recommended to discuss the liner requirements with the manufacturer and once a product has been selected, to discuss the technical specifications with the NRCB.

Pumping may be required during liner placement if the excavation starts to fill with groundwater. It is recommended that the means be available to prevent "bubbling" of the liner if groundwater starts to form below the liner in the catch basin footprint.

Seepage and sloughing may be encountered in the till subgrade depending upon the base elevation of the catch basin.

If a synthetic liner is utilized, the NRCB requires the bottom of the liner to be equal or greater than 1.0 m from the groundwater table at the time of construction.



6.6 QUALITY CONTROL / QUALITY ASSURANCE

As part of the quality control program, it is recommended that a geotechnical engineer or representative be on-site to inspect the excavation and compaction required. The geotechnical engineer will be able to provide immediate on-site recommendations to potential difficulties that may arise during construction.

6.7 INLET PIPE

It is understood multiple inlet pipes will be utilized for the construction of the catch basin. The inlet pipes must be sealed to ensure liquid manure doesn't seep back along the pipe extrusion, creating a potential source of contamination. Bentonite chips or concrete are typically utilized around the inlet pipe to create the required seal.

6.8 EROSION

Due to the catch basin's size or liner type, these measures may not be necessary, but unchecked erosion can lead to slope and berm failure and erosion preventative measures may be required. Placing riprap is normally the most cost effective erosion protection material, placed on the waterward side, due to its effectiveness, durability and availability.

Additionally, exposed soil should be graded to the required slope, overlain with topsoil, and seeded or hydroseeded with grass. Trees and shrubs planting is not recommended as tree roots detrimentally affect berms by root penetration and shrubs cause obstructions in viewing piping, seepage, and burrowing animals. The vegetation will serve to protect the upper portions of the slope from erosion by surface runoff water and will also increase the stability of the slope. The grass should be trimmed regularly as to not obstruct the inspectors view.

6.9 FENCE

It is recommended that continuous fencing around the perimeter of the catch basin is constructed. A fence will help prevent unauthorized entry to the catch basin and will also help reduce the detrimental effects of burrowing animals such as beavers, muskrats, gophers, etc.



6.10 INSPECTIONS

It is the responsibility of the owner to conduct routine and periodic inspections and to maintain and repair the catch basin to acceptable standards. It is recommended that the catch basin is inspected on a regular basis or as per the Natural Resources Conservation Board. The inspector shall note, but not be limited to noting, the presence or absence of settlement, seepage, burrowing animals, erosion, freeboard level, erosion protection performance and condition, fence condition, vegetation growth that my lead to a decreased performance of the liner, and general berm and catch basin condition.

7 CLOSURE

Union Street Geotechnical Ltd. prepared this report for the exclusive use of Eagle Builders LP, and their agents, to aid in the design and construction of the proposed Double T Cattle Co. feedlot located within the N.W. ¼ of 15-42-25 W4 in Ponoka County, Alberta. The content reflect Union Street's best judgement available to it at the time of preparation. Any use which a third party makes of this report, or any reliance on, or decisions to be made based on it, are the responsibility of such third party and Union Street accepts no responsibility for damages, if any, suffered by any third party as a result of decisions made or actions based on this report.

Our recommendations and conclusions are based upon the information obtained from the subsurface exploration. The borings and associated laboratory testing indicate subsurface conditions only at the time and to the depth, of the specific boring location investigated and only for the soil properties tested. The subsurface conditions may vary between the boreholes and over time. The interpretation of subsurface conditions provided is a professional opinion of encountered conditions and is not a certification or guarantee of site conditions. If variations, or other latent conditions become evident, Union Street should be notified immediately so that our conclusions and recommendations can be re-evaluated. Although subsurface conditions have been explored, we have not conducted investigations, sampling, field or laboratory testing, evaluations, or modelling of the site or subsurface conditions with respect to the presence of contaminated soil or groundwater or slope stability conditions.



This report contains the results of our geotechnical investigation as well as certain recommendations arising from our investigation. The general recommendations herein do not constitute a design, in whole or in part, of any of the structural elements of the proposed work. Incorporation of any or all of our general recommendations into the design of any such element does not constitute us as designers or co-designers of such elements, nor does it mean that such design is appropriate in geotechnical terms. The designers of such elements must consider the appropriateness of our general recommendations in light of all design criteria known to them, many of which are not known by us. Our mandate has been to perform a geotechnical investigation and provide general site suitability recommendations, which we have completed by means of this report. We have had no mandate to design, or review the design of any elements of the proposed work and accept no responsibility for such design or design review.

This report has been prepared in accordance with generally accepted geotechnical engineering practice common to the local area. No other warranty, expressed or implied, is made.

This document, and the information contained within, are the confidential property of Eagle Builders LP and any disclosure of same is governed by the provisions of each of the applicable provincial or territorial Freedom of Information legislation, the Privacy Act (Canada) 1980-81-82-83, c.111, Sch. II "2", and the Access to Information Act (Canada) 1980-81-82-83, c.111, Sch. I "1", as such legislation may be amended or replaced from time to time.



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Yours truly,

Union Street Geotechnical Ltd.

Prepared By:

Neil Tomaszewski, E.I.T. Project Engineer



Union Street Geotechnical Ltd. APEGA Permit No. P12644

1

7th October, 2021 APEGA ID# 80317



ATTACHMENTS

DRAWINGS

Drawing No. A1 - Site Location Plan Drawing No. A2 - Borehole Location Plan

PHOTOGRAPHS

Photographs No. 1 & 2

BOREHOLE LOGS

Boreholes No. BH101 to BH109, inclusive

LABORATORY TEST RESULTS

Flexible Wall Permeameter - Sample No. MW16 Flexible Wall Permeameter - Sample No. MW48 Laboratory Hydrometer - Sample No. MW7





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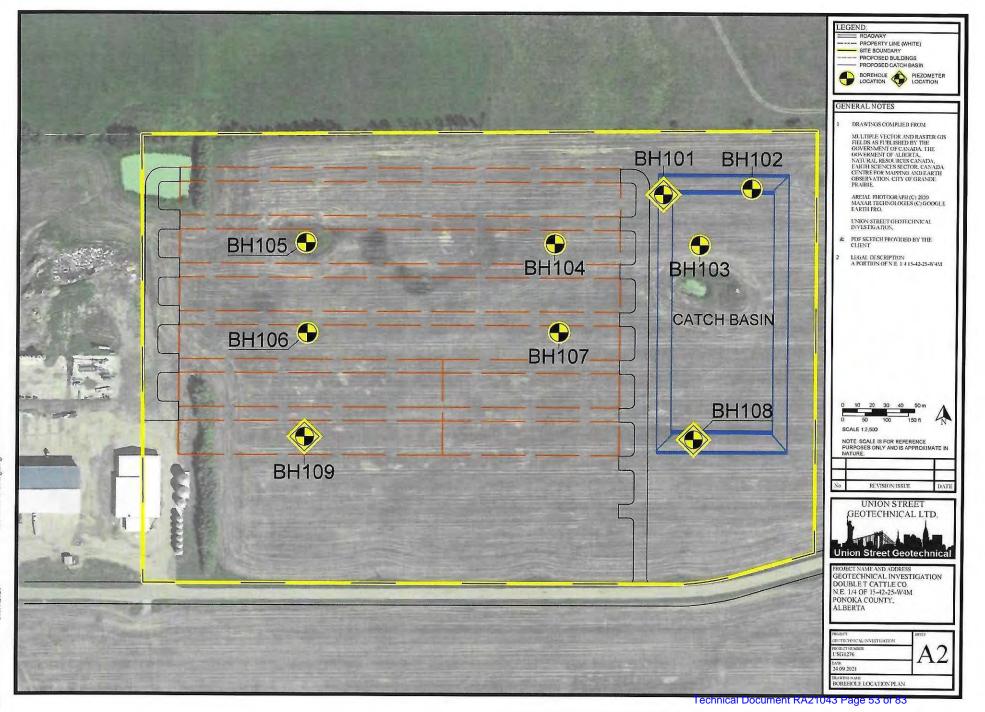
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USG1276 - Drawing dwg

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Photographs - Geotechnical Investigation N.W. ¼ of 15-42-25 W4 Ponoka County, Alberta



Photograph No. 1: Photograph taken from near the western edge of the proposed feedlot, facing east, showing the proposed feedlot footprint, site grading, agricultural land, and general site conditions observed at the time of drilling. Photograph taken on the 14th September, 2021.



Photograph No. 2: Photograph taken from near the eastern edge of the proposed feedlot, facing west, showing the proposed feedlot footprint, site grading, agricultural development to the west-southwest, and general site conditions observed at the time of drilling. Photograph taken on the 14th September, 2021.



Borehole Logs

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		FIELD BC	REHC	LE I	_OG		-	1	E	UREH(DLE NU BH101	
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DEPTH (m)	ПТНОГОСУ	DESCRIPTION	ТҮРЕ	SAMPL	E "N" TdS	POCKET PEN (kPa)	MOISTURE CONT. (%)	SULPHATE (%)	USC	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	WELL INSTALLATION
1.0 -							-	07				
0.0 - - 1.0 - 2.0 -		TOPSOIL: 356 mm thick. TILL: Clay, silty, sandy. Very dark brown (10YR 2/2). Oxidized. Moist. Stiff to very stiff. Massive. Coal chip, gravel, and silt pocket inclusions. Calcareous.		MW1 MVV2 MVV3	12	192 132 96	11.8 16.0 16.5		СН	51.9	11.8	Solid 25 mm PVC casing.
3.0 -		MUDSTONE: Silty, clayey, some	******** ********	MW4	19	96	19.7					
4.0 -		sand. Dark grey (10YR 4/1). Non- oxidized. Dry to moist. Very stiff to hard. Massive. Calcareous.	******	MVV5	Ref.	144 215	16.0 15.4		СН	55.0	19.5	Auger cuttings.
5.0 -		@ 5.33 m, trace sand.	××××××××	MW7		-	15.1					
5.0 -		@ 7.62 m, seepage.	******* ******** *******	MVV8	Ref.	144	15.1					Hand
7.0 - - 3.0 -		NOTES: End of borehole at 7.93 m below surface. Seepage, but no sloughing encountered during drilling. Piezometer installed, annulus backfilled to surface with auger cuttings. Water level at 2.47 m below grade on 28 September, 2021.	x^x^x^x^x	MVV9 MVV10 MVV11	Ref.	- 96 48	20.9 17.6 23.3					slotted 2 mm PVC

	FIELD BOI	FIELD BOREHOLE LOG							OREHC	DLE NU BH102	
PROJECT NUMBE	R: USG1276			-		CA	SING	STICKL	-	ып 102	N/A
ROJECT NAME:	Geotechnical Investigation						TAL D				9.14 m
OCATION:	N.W. 1/4 of 15-42-25 W4, Pone	oka Coun	tv. Albe	rta						EVAT	ON: N/A
CLIENT:	Eagle Builders LP	onu coun	cy, moe	i ta		01	+	oora.			ON. IVA
	D: 150 mm Solid Stem Auger										1
OGGED BY:	M.W.						1	_	with	1.	
DATE BEGUN:	14 September, 2021							Th			
	D: 14 September, 2021					l	Jnio	n St	reel	Ge	otechnica
	,	5	SAMPLE								
DEPTH (m) LITHOLOGY	DESCRIPTION	ТҮРЕ	No.	"N" TdS	POCKET PEN (kPa)	MOISTURE CONT. (%)	SULPHATE (%)	nsc	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	WELL INSTALLATION
0.0 1 TOF	SOIL: 356 mm thick.	T									0.7
1.0 - yello brow Very	.: Clay, silty, some sand. Dark wish brown (10YR 4/4) to dark yn (10YR 3/3). Oxidized. Moist. y stiff. Massive. Coal chip,		MW12		192	10.2					00000 00000
2.0 – Calc	el, and silt pocket inclusions. areous.		MW14		144	15.7					
3.0 -											00000
4.0 - @ 4.	88 m, seepage.		MW15		-	15.7					Ora Ora Auger
5.0			MW16		-	16.1					Circle cuttings.
trace	DSTONE: Silt, clayey, some to e sand. Dark grey (10YR 4/1). -oxidized. Dry to moist. Very to hard. Massive. Calcareous.		MW17		-	26.1					0000
7.0			MW18		- <u>1</u>	27.9					000
8.0											2000 201 200 200 200 200 200 200 200 200
9.0 / belo slou	ES: End of borehole at 9.14 m w surface. Seepage and ghing encountered during ng. Borehole backfilled to		MW19		-	29.2					SOS OS
	ace with auger cuttings.										
0.0		<u> </u>		2							

	FIELD BOF	REHC	DLE L	OG				B(DREHO	LE NUI 3H103	
T NUMBER: U								STICKU			N/A
	eotechnical Investigation			22			TAL DI				9.14 m
	.W. 1/4 of 15-42-25 W4, Pono	ka Coui	nty, Albe	rta		GF		SURF	ACE EL	EVAII	ON: N/A
	agle Builders LP						L.				
	50 mm Solid Stem Auger I.W.									1 -	
	1. vv. 4 September, 2021					100		Th			
	4 September, 2021 4 September, 2021					J	Jnio	n St	reet	Geo	otechnical
			SAMPLE								
LIIHOLOGY	DESCRIPTION	ТҮРЕ	No.	"N" TqS	POCKET PEN (kPa)	MOISTURE CONT. (%)	SULPHATE (%)	USC	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	WELL INSTALLATION
			11								
TOPSOI	L: 305 mm thick.		in the second se								0.0
	ay, silty, some sand.										0
Yellowis grey (10 Hard. Ma	YR 4/1). Oxidized. Moist. assive. Coal chip, gravel, pocket inclusions.		MW20		215	12.0					00000
Calcared	ous.										0.0
			MW21		215	17.8					0.0
trace sau grey (10	DNE: Silt, clayey, some to nd. Grey (10R 5/1) to dark YR 4/1). Non-oxidized. Dry Very stiff to hard. Massive.										00000
Calcared	ous.		MW22		-	14.8					Auger Carcuttings.
			MW23		-	15.7					
 @ 7.62 m	n, seepage.		MW24		-	28.8					000
			MW25		-	29.9					00000 1 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
below su sloughin drilling. E	End of borehole at 9.14 m inface. Seepage and g encountered during Borehole backfilled to with auger cuttings.										

DCATION: M LIENT: F RILLING METHOD: 1	Geotechnical Investigation N.W. 1/4 of 15-42-25 W4, Pono Gagle Builders LP 50 mm Solid Stem Auger	ka Cour	nty, Albe	erta		тс	ASING S DTAL DI ROUND	EPTH:	JP:	BH104 .EVATI	N/A 4.57 m ON: N/A
ATE BEGUN: 1	4.W. 4 September, 2021						l	1			
ATE COMPLETED: 1							Jnio	n Si	reef	Ge	otechnica
DEPTH (m)	DESCRIPTION		SAMPLE		POCKET PEN (kPa)	MOISTURE CONT. (%)	SULPHATE (%)		LIQUID LIMIT (%)	PLASTIC LIMIT (%)	WELL
		ТҮРЕ	N	SPT "N"	0Ct	NOIS	SULP	usc	INDI-	LAS ⁻	
.0 - TILL: Cla Yellowis greyish I Oxidized Coal chi inclusion .0 - MUDST trace sar Non-oxid stiff to ha sloughin drilling. E	L: 356 mm thick. ay, silty, some sand. h brown (10YR 5/6) to dark brown (10YR 4/2). I. Moist. Very stiff. Massive. o, gravel, and silt pocket as. Calcareous. DNE: Silt, clayey, some to nd. Pale Brown (10YR 6/3). dized. Dry to moist. Very ard. Massive. Calcareous. End of borehole at 4.57 m arface. No seepage or g encountered during Borehole backfilled to with auger cuttings.		MW26 MW27 MW28		144	9.4 15.5 20.2					Auger cuttings.

	FIELD BO	REHO	DLE L	.0G		-		В		DLE NU BH105	
ROJECT NU	UMBER: USG1276					CA	SING	стіскі	20 10 11 10 10 10 10 10 10 10 10 10 10 10	DITIOS	N/A
ROJECT N/ OCATION: LIENT: PRILLING MI OGGED BY ATE BEGUI	N.W. 1/4 of 15-42-25 W4, Por Eagle Builders LP ETHOD: 150 mm Solid Stem Auger : M.W.		nty, Albe	rta		TC GF		EPTH: SURF	ACE E		4.57 m ON: N/A
ATE COMP	LETED: 14 September, 2021			_			Jnio	on Si	tree	t Ge	otechnica
DEPTH (m) LITHOLOGY	DESCRIPTION	ТҮРЕ	SAMPLE	SPT "N"	POCKET PEN (kPa)	MOISTURE CONT. (%)	SULPHATE (%)	USC	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	WELL INSTALLATION
0.0			1 1						F		
1.0 -	TOPSOIL: 305 mm thick. TILL: Clay, silty, sandy. Brown (10YR 4/3). Oxidized. Moist. Hard. Massive. Coal chip, gravel, and silt pocket inclusions. Calcareous.		∃MW29		215	11.4		СН	52.4	11.3	00000000000
3.0	MUDSTONE: Silt, clayey, some to trace sand. Dark grey (10YR 4/1). Non-oxidized. Dry to moist. Stiff to hard. Massive. Calcareous.		MW30 MW31		96	24.1					Auger cuttings.
5.0 - 6.0 -	NOTES: End of borehole at 4.57 m below surface. No seepage or sloughing encountered during drilling. Borehole backfilled to surface with auger cuttings.										
7.0 -											
8.0 — - 9.0 —											
0.0											

		FIELD BO	REHC	DLE L	.OG		-		B		LE NU BH106	MBER
PROJECT		R: USG1276			1000		CA	SING	STICKL			N/A
ROJECT OCATIO		Geotechnical Investigation N.W. 1/4 of 15-42-25 W4, Pon Eacle Builders I B	ioka Cour	nty, Albe	rta					ACE EL	.EVATI	4.57 m ON: N/A
	METHO	Eagle Builders LP D: 150 mm Solid Stem Auger										
		M.W.						I	-	11		
DATE BE		14 September, 2021										
DATE CO	MPLETE	D: 14 September, 2021	1			1		סוווכ	<u> </u>	reel	Ge	otechnica
DEPTH (m)		DESCRIPTION	ТҮРЕ	SAMPLE	SPT "N"	POCKET PEN (kPa)	MOISTURE CONT. (%)	SULPHATE (%)	nsc	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	WELL INSTALLATION
	3		-1	ž	S	ă	Σ	S	5		Ц	
0.0		PSOIL: 305 mm thick.										0
1.0 -	brov Stiff	L: Clay, silty, sandy. Yellowish wn (10YR 5/6). Oxidized. Moist. to very stiff. Massive. Coal a, gravel, and silt pocket usions. Calcareous.		MW32		96	12.6					000000 2000000
2.0	@ 0.	76 m, sand seam, 0.30 m thick.		MW33		144	18.0					Auger Creatings.
4.0	- <u></u> - trac - <u></u> 7/4)	DSTONE: Silt, clayey, some to e sand. Very pale brown (10YR . Non-oxidized. Dry to moist. d. Massive. Calcareous.		∃MW34		-	16.5					
5.0 -	belo slou drilli	TES: End of borehole at 4.57 m w surface. No seepage or ghing encountered during ng. Borehole backfilled to ace with auger cuttings.										
6.0 -		0										
-												
7.0 -												
8.0 -												
9.0 -												
-												
10.0						I	l	1				l

			FIELD BO	REHC	DLE L	.OG		-		B	OREHO	DLE NU BH107	
PROJ	ECT N	UMBER:	USG1276					CA	SING S	STICK	UP:	01107	N/A
OCA			Geotechnical Investigation N.W. 1/4 of 15-42-25 W4, Pon Eagle Builders LP 150 mm Solid Stem Auger	oka Cour	nty, Albe	erta		тс	TAL D	EPTH:		LEVATI	4.57 m ION: N/A
	ED BY		M.W.						. I	-	11		
	BEGU		14 September, 2021										
DATE		LETED:	14 September, 2021				1	1	OIIIO	n s	tree	t Ge	otechnica
DEPTH (m)	ГІТНОГОСУ		DESCRIPTION	ТҮРЕ	SAMPLE	SPT "N"	POCKET PEN (kPa)	MOISTURE CONT. (%)	SULPHATE (%)	USC	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	WELL INSTALLATION
0.0 -												1	<u>, , , , , , , , , , , , , , , , , , , </u>
1.0 - - 2.0 -		TILL: (greyis Oxidiz Coal c	OIL: 305 mm thick. Clay, silty, sandy. Dark h brown (10YR 4/2). ed. Moist. Hard. Massive. hip, gravel, and silt pocket ons. Calcareous.		MVV35		215	12.2		CI	40.1	13.0	
- 3.0 —		silt.	? m, sand, some clay, some		MW36		48	19.2					Auger C. cuttings.
4.0 -		trace s Non-o	TONE: Silt, clayey, some to sand. Dark grey (10YR 4/1). xidized. Moist. Stiff to hard. ve. Calcareous.		MW37		96	16.6					
5.0 —		below slough drilling	S: End of borehole at 4.57 m surface. No seepage or ing encountered during Borehole backfilled to e with auger cuttings.										
6.0 -													
7.0 -													
8.0 —													
9.0 -													
10.0 -													
													Page 1 of 1 Page 63 of 83

		FIELD BC	REHC	LE L	.OG				B	OREHC	DLE NU BH108	
PROJ	ECT N	UMBER: USG1276					CA	SING	STICKL		50108	0.88 m
PROJ	ECT N	AME: Geotechnical Investigation						TAL D				0.88 m 9.14 m
	TION:	N.W. 1/4 of 15-42-25 W4, Po	noka Cour	ity, Albe	rta					ACE EI	EVATI	ION: N/A
	IT:	Eagle Builders LP					0.	1	0011			
ORILL	ING M	ETHOD: 150 mm Solid Stem Auger						Ľ.				1
	ED BY								-		1.	
DATE	BEGU	N: 14 September, 2021										
DATE	COMP	LETED: 14 September, 2021						Jnio	n St	treet	t Ge	otechnica
				SAMPLE	E		MOISTURE CONT. (%)					
						РОСКЕТ РЕN (kPa)	LT.	~		(%	PLASTIC LIMIT (%)	
(¥	DESCRIPTION				N	CO U	(%)		LIQUID LIMIT (%)	TIM	
DEPTH (m)	гітногоду	DESCRIPTION			=		URE	SULPHATE		LIZ		WELL INSTALLATION
PTH	IOH.		ΓΥΡΕ		SPT "N"	- Hereit	IST	Ha-	G	an	STI	
DE	5		ĮΣ	No.	SP.	PO	MO	SUI	nsc	P	PLA	
1.0												
-1.0												E Cap.
-												
0.0	<u>لاً ب</u>							1				
-		TOPSOIL: 305 mm thick.										
1.0 -		TILL: Sand, some clay, some silt.		MW38		_	10.4					
1.0		Brownish yellow (10YR 6/8). Oxidized. Moist. Loose. Massive.					100 H 10 UK					
1	<u> </u>	Calcareous.	1									
2.0 -	$\frac{1}{2}$	MUDSTONE: Silt, clayey, some to										
-	<u>. </u>	trace sand. Light yellowish brown (10YR 6/4) to grey (10YR 5/1). Non		MW39		-	4.8					
3.0 -	<u> </u>	oxidized. Moist. Hard. Massive.	-									Solid 25
	<u> </u>	Calcareous.										casing.
	<u> </u>	-										
4.0 -	<u></u> .			MW40		-0	12.9					
+	$\frac{1}{1}$			NAVA/44								Auger Cuttings.
5.0 -	÷±÷			MW41		<u>-</u>	14.0					cuttings.
ļ				MW42		-	16.2					
	<u> </u>						10.2					
6.0 -	<u></u>											
4	<u></u>											
7.0 -	<u></u>			MW43		2	14.6					
ļ	<u></u> -											
	<u>i</u> ii:	NOTES: End of borehole at 9.14 m	7									Hand
8.0 -	÷÷÷	below surface. No seepage or										slotted 25
+	<u></u>	sloughing encountered during drilling. Piezometer installed,		MW44		. 	12.0					
9.0 -	- <u>-</u>	annulus backfilled to surface with										
_		auger cuttings. Water level at 2.68 m below grade on 28 September,										
10.0		2021.										
0.0 ⊥												
				-								Page 1 of 1 Page 64 of 83

	FIELD BO	REHC	OLE L	.0G		-		B		DLE NU BH109	JMBER
PROJECT NA LOCATION: CLIENT: DRILLING ME LOGGED BY: DATE BEGUN	N.W. 1/4 of 15-42-25 W4, Pon Eagle Builders LP ETHOD: 150 mm Solid Stem Auger M.W.	1				TC GF		EPTH: SURF			0.85 m 4.57 m ION: N/A otechnica
DEPTH (m) LITHOLOGY	DESCRIPTION	ТҮРЕ	SAMPLE o Z	SPT "N"	POCKET PEN (kPa)	MOISTURE CONT. (%)	SULPHATE (%)	usc	LIQUID LIMIT (%)	PLASTIC LIMIT (%)	WELL INSTALLATION
4.0	TOPSOIL: 305 mm thick. TILL: Sand, some clay, some silt. Yellowish brown (10YR 5/8). Oxidized. Moist. Compact. Massive. Calcareous. MUDSTONE: Clay, silty, trace sand. Dark grey (10YR 4/1). Non- oxidized. Moist. Hard. Massive. Calcareous. NOTES: End of borehole at 4.57 m below surface. No seepage or sloughing encountered during drilling. Piezometer installed, annulus backfilled to surface with auger cuttings. Water level at 2.63 m below grade on 28 September, 2021.		MW45 MW46 MW47 MW48 MW49			15.1 - 15.3 24.5 13.4					Cap. Solid 25 mm PVC casing.



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Project Name: Depth: 4.57 m Project Number: USG1276 Testing Company: Union Street Geo. Client: Field Technician: M.W. Testhole: BH102 Sample Date: Location: Lab Technician: B.B. Sample Number: MW6 Date Tested: September 18, 2021

Flexible Wall Permeameter (ASTM D5084-10)

Standard Test Method for Measurement of Hydraulic Conductivity of Saturated Porous Materials Using a Flexible Wall Permeameter

Material and Test Description

	Material	Description:
--	----------	--------------

Clay Till - silty, some sand, trace gravel, oxide inclusion, coal, alkalines, dark grey

Test Type:	Constant Head	Remould	ng Details	
Mould Size:	Flexible Wall	Max Dry Density (kg/m ³):	-	
Sample Source:	Shelby Tube	Proctor ID:	-	
Fluid Used:	Deaired Water	Percent Max (%):	-	
Fluid Reservoir:	Burrettes	Target Dry Density (kg/m ³):	-	

Water Con	tent			Sample Siz	е	10 C	
Wet + Tare (g):	434.2	Trial	1	2	3	4	Average
Dry + Tare (g):	379.1	Diameter (mm):	73.1	72.6	72.6	73.1	72.9
Tare (g):	14.1	Length (mm):	79.4	79.3	79.2	79.4	79.3
Water Content (%):	15.1%	Weight (g)			723.7		1

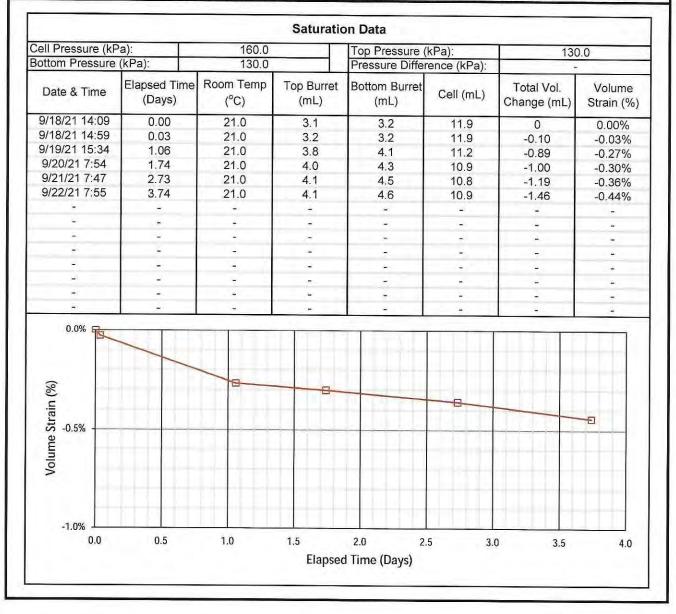
Area (cm ²):	41.7	Specific Gravity (Note 2):	2.72
Volume (cm ³):	330.6	Void Ratio:	42.9%
Wet Density (kg/m ³):	2189	Saturation:	95.6%
Dry Density (kg/m ³):	1902	Porosity:	30.0%

		Final Sample C	haracteristics	5					
Water Con	tent			Sample Size	е		- No		
Wet + Tare (g):	748.5	Trial	1	2	3	4	Average		
Dry + Tare (g):	644.1	Diameter (mm):	73	73.2	73.1	73.7	73.3		
Tare (g):	13.1	Length (mm):	79.9	79.8	79.9	79.9	79.9		
Water Content (%):	16.5%	Weight (g)		735.6					
Area (cm²):		42.1	Specific Gravi	ty (Note 1):		2.72			
Volume (cm ³):		336.6	Void Ratio:		44.9%				
Wet Density (kg/m ³):		2185	Saturation:	Saturation:			100.0%		
Dry Density (kg/m ³):		1875	Porosity:			31.0%			

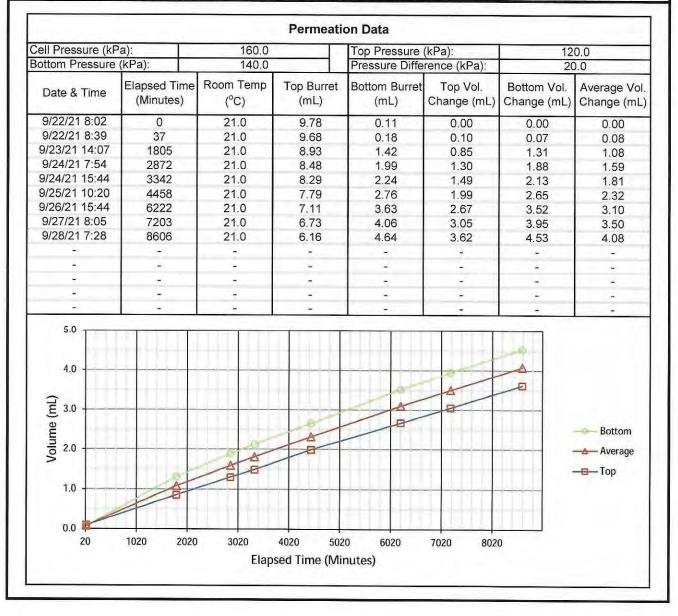
Note 1: Specific gravity for final sample characteristics calculation adjusted to result in 100.0% saturation.

Note 2: Specific gravity for initial sample characteristics calculation set equal to that of the final.

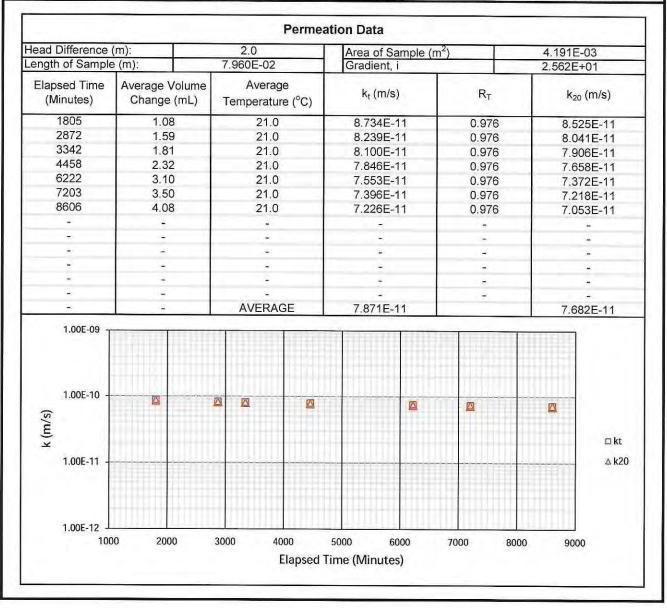
Testing	
Testing Company:	Union Street Geo.
Field Technician:	M.W.
Sample Date:	
Lab Technician:	B.B.
Date Tested:	September 18, 2021
	Field Technician: Sample Date: Lab Technician:



Project Name:		Depth:	4.57 m
Project Number:	USG1276	Testing Company:	Union Street Geo.
Client:		Field Technician:	M.W.
Testhole:	BH102	Sample Date:	
Location:		Lab Technician:	B.B.
Sample Number:	MVV16	Date Tested:	September 18, 2021



Depth:	4.57 m
Testing Company:	Union Street Geo.
Field Technician:	M.W.
Sample Date:	
Lab Technician:	B.B.
Date Tested:	September 18, 2021
	Testing Company: Field Technician: Sample Date: Lab Technician:



Project Name: Depth: 3.05 m Project Number: USG1276 Testing Company: Union Street Geo. Client: Field Technician: M.W. Testhole: BH109 Sample Date: Location: Lab Technician: B.B. Sample Number: **MW48** Date Tested: September 18, 2021

Flexible Wall Permeameter (ASTM D5084-10)

Standard Test Method for Measurement of Hydraulic Conductivity of Saturated Porous Materials Using a Flexible Wall Permeameter

Material and Test Description							
Material Description:							
Sandy Clay							
Test Type:	Constant Head	Remould	ling Details				
Mould Size:	Flexible Wall	Max Dry Density (kg/m ³):	-				
Sample Source:	Shelby Tube	Proctor ID:	-				
Eluid Heedu			the second				
Fluid Used:	Deaired Water	Percent Max (%):	-				

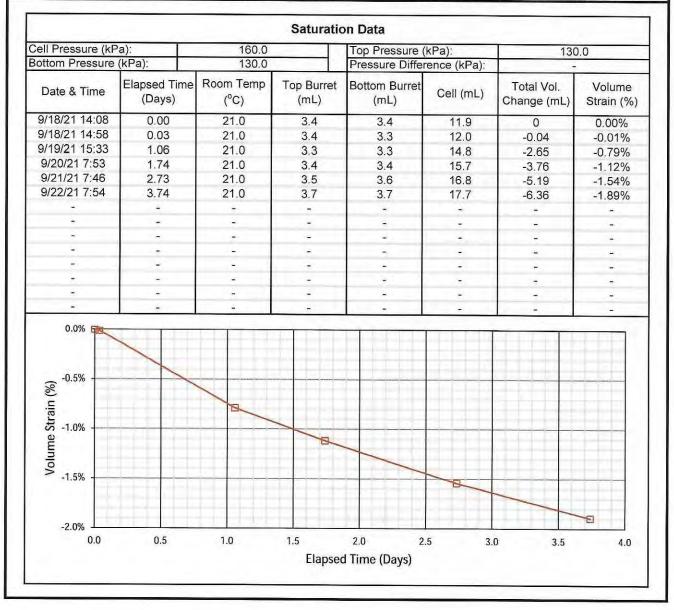
Water Con	itent			Sample Siz	е		
Wet + Tare (g):	607.6	Trial	1	2	3	4	Average
Dry + Tare (g):	490.7	Diameter (mm):	73.4	73	72.9	72.8	73.0
Tare (g):	14.0	Length (mm):	80.3	80.2	80.4	80	80.2
Water Content (%):	24.5%	Weight (g)			651.3		1

Area (cm ⁻):	41.9	Specific Gravity (Note 2):	2.68
Volume (cm ³):	336.0	Void Ratio:	72.4%
Wet Density (kg/m ³):	1938	Saturation:	90.9%
Dry Density (kg/m ³):	1557	Porosity:	42.0%

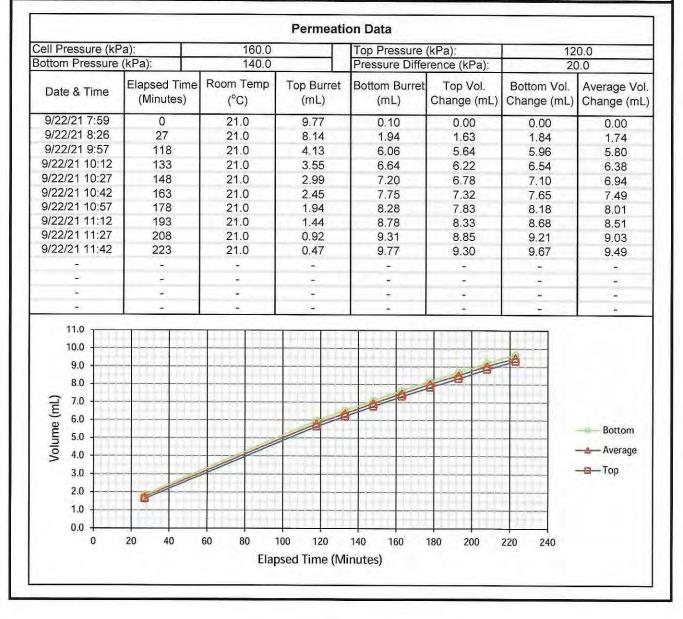
Water Con	tent		Sample Size				
Wet + Tare (g):	864.4	Trial	1	2	3	4	Average
Dry + Tare (g):	732.4	Diameter (mm):	73.1	71.9	72.4	73.0	72.6
Tare (g):	199.6	Length (mm):	80.2	80.1	80	80.2	80.1
Water Content (%):	24.8%	Weight (g)			667.1		
Area (cm²):		41.4	Specific Gravi	ty (Note 1):	-	2.68	
Volume (cm ³): 331.7		331.7	Void Ratio: 66.5%			6	
Wet Density (kg/m ³):			Saturation: 100.0%			%	
Dry Density (kg/m ³): 1612		Porosity: 39.9%				6	

Note 1: Specific gravity for final sample characteristics calculation adjusted to result in 100.0% saturation. Note 2: Specific gravity for initial sample characteristics calculation set equal to that of the final.

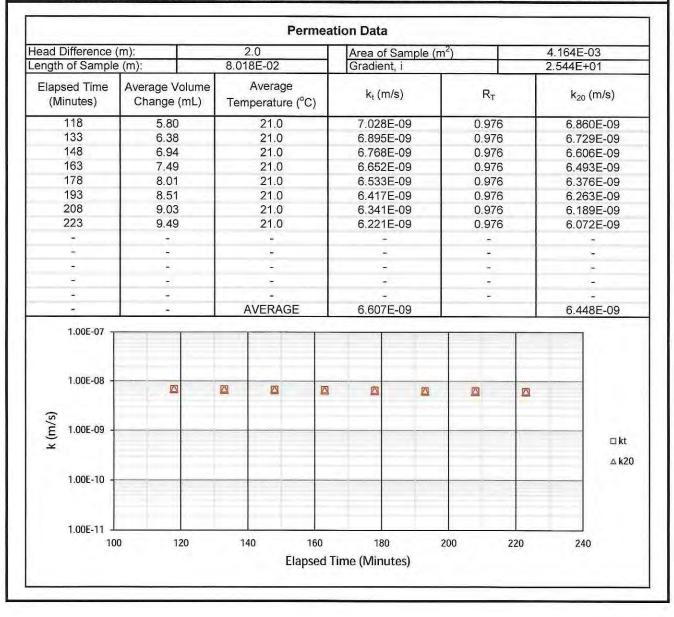
Project Name:	Depth:	3.05 m
Project Number: USG1276	Testing Company:	Union Street Geo.
Client:	Field Technician:	M.W.
Testhole: BH109	Sample Date:	
Location:	Lab Technician:	B.B.
Sample Number: MW48	Date Tested:	September 18, 2021

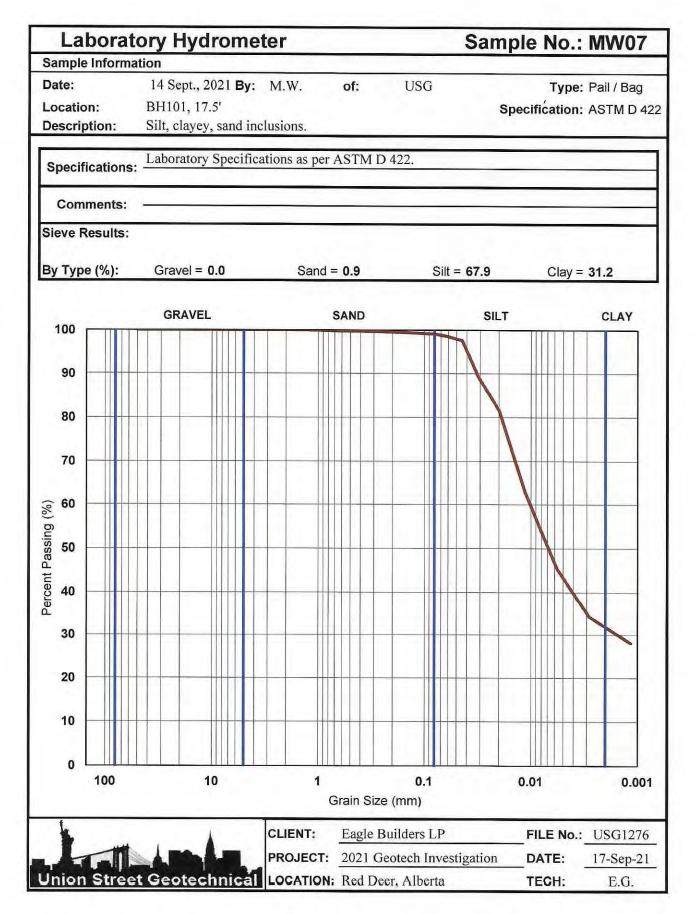


Depth:	3.05 m
Testing Company:	Union Street Geo.
Field Technician:	M.W.
Sample Date:	
Lab Technician:	B.B.
Date Tested:	September 18, 2021
	Testing Company: Field Technician: Sample Date: Lab Technician:



Project Name:		Depth:	3.05 m
Project Number:	USG1276	Testing Company:	Union Street Geo.
Client:		Field Technician:	M.W.
Testhole:	BH109	Sample Date:	
Location:		Lab Technician:	B.B.
Sample Number:	MW48	Date Tested:	September 18, 2021





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March 7, 2022

Jeff Froese NRCB Approval Officer Red Deer, AB jeff.froese@nrcb.ca

RE: Eagle Builders – Double T Cattle Feedlot – Application RA21043 – NE 15-42-25 W4

Thank you for your email request on this file regarding the storage volume of the proposed irregular shape catch basin.

As shown in Figure 1, the Al-Terra engineering report lists a HWL volume of 9650m³ at a liquid elevation of 864.0m.

Methodology

The chosen methodology to determine the storage volume is to "split" the irregular shape into two rectangular shapes, and calculate the volume for each shape (Figure 1):

- 1. Large, west rectangle. Dimensions would be:
 - a. Length of 128.38m (at 864.5m)
 - b. Width of 56.64m (at 864.5m)
- 2. Small, east rectangle. Dimensions would be:
 - a. Length of 52.21m (108.85 56.64), (at 864.5m)
 - b. Width of 21.99m (at 864.5m)
- 3. For both rectangles, common dimensions are:
 - a. Top of berm 864.5m
 - b. Liquid top 864.0m
 - c. Pond bottom is 862.5m
 - d. Freeboard depth is 0.5m
 - e. Total volume (including freeboard) is calculated using a depth of 2.0m
 - f. Usable volume (excluding freeboard) is calculated using a liquid depth of 1.5m
 - g. Interior side slopes are 3:1 (horizontal to vertical)

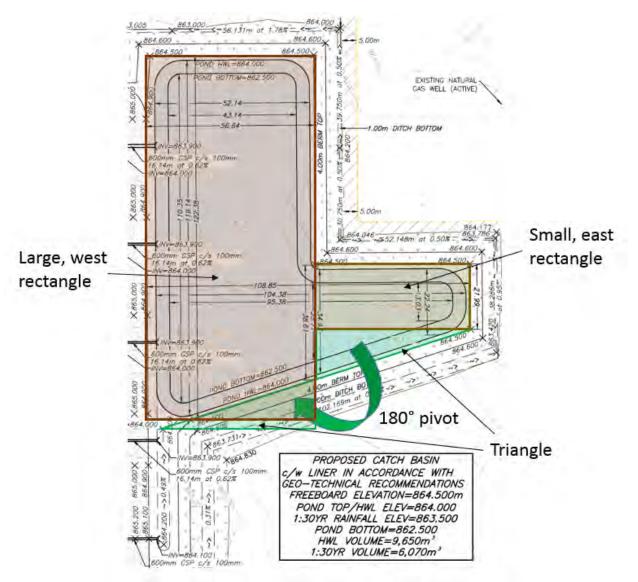


Figure 1. Irregular shape catch basin. Al-Terra Engineering (Red Deer) Ltd., Site Grading Plan Sheet C02. #5, 2022-02-23. Color shading and labels added.

Assumptions

Assumptions and their anticipated effects on the calculations:

- Rounded corners shown are calculated as "square".
 - This would result in a catch basin volume calculation being slightly larger than the actual catch basin volume.
- Angled catch basin slope on the southeast is split in approximately half, at the intersection of a line that would extend south from the interior berm east top of the large, west rectangle. The triangle on the east side of this slope (and south of the small, east rectangle) would pivot 180 degrees, and be added to the south east corner of the large, west rectangle. "Moving" this portion of the irregular shape catch basin would result in the dimensions of the two rectangles listed.

- As a portion of the triangle is shown beyond the dimensions of the large, west rectangle (Figure 1), this would result in a catch basin volume calculation being slightly smaller than the actual catch basin volume.
- Catch basin dimensions at west edge of entire catch basin are measured to gravel road (at 864.9m), rather than the catch basin top (at 864.5m) on the other sides.
 - This would result in a catch basin volume calculation slightly larger than the actual catch basin volume.
- Calculating the volume of two catch basins suggests that a "berm" (with 3:1 H to V side slopes) would be between them, when in fact the "berm" volume would be usable catch basin volume.
 - This would result in a catch basin volume calculation slightly smaller than the actual catch basin volume.

Calculations

Volume calculations of the rectangles were made using a calculator published by Alberta Agriculture, Food and Rural Economic Development (<u>https://www.agric.gov.ab.ca/app19/loadcatchbasin</u>)¹. Results for 1.5m of liquid storage (liquid elevation of 864.0m) for the large, west rectangle and small, east rectangle are shown in Appendix A, and are:

- 1. Large, west rectangle volume = 8885 m³ usable volume (excluding freeboard)
- 2. Small, east rectangle volume = 976 m³ usable volume (excluding freeboard)
- 3. Total = 9861 m³ usable volume (excluding freeboard)

Conclusion

Al-Terra provided a volume of 9650m³ at a liquid elevation of 864.0m. The total usable volume (excluding freeboard) using the two rectangles method was calculated to be 9861 m³. The slightly larger volume calculation associated with the two rectangles method is likely to be the net result of the four assumptions.

It is reasonable to use the Al-Terra volume of 9650m³ as the usable volume (excluding freeboard) of the irregular shape catch basin.

If you have any questions, please contact me.

Scott Cunningham Scott Cunningham, P.Eng., P.Ag.

Scott Cunningham, P.Éng., P.Ag. NRCB Environmental Specialist Red Deer, AB scott.cunningham@nrcb.ca

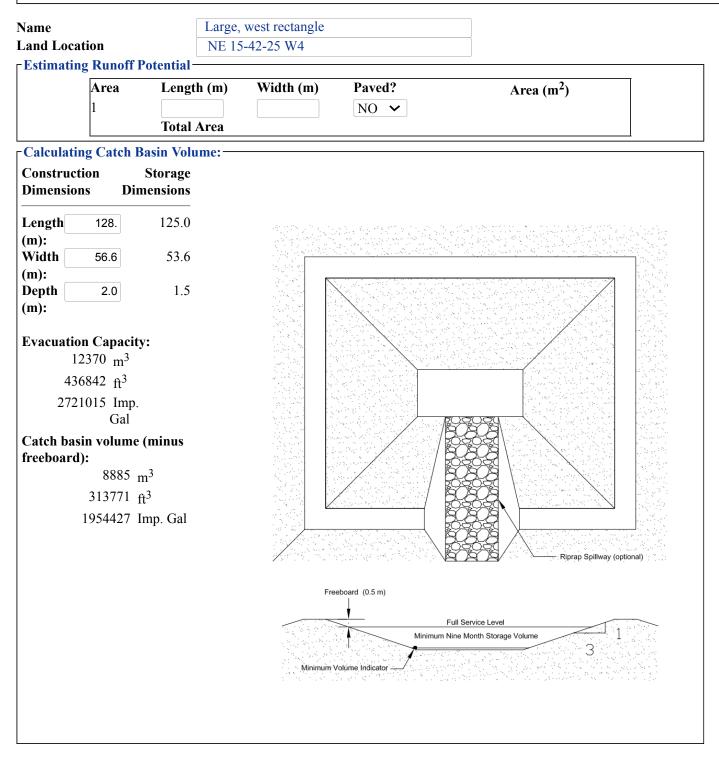
¹ Runoff potential was calculated separately because too many assumptions would have been necessary to determine the portion of the feedlot draining to the large, west and small, east rectangles. Therefore, runoff potential calculations were not included in Appendix A.

2/25/22, 11:14 AM



Catch Basin Dimension Calculator

For more information on runoff control catch basin design consideration including liner options, catch basin protection, etc., check out the catch basin <u>factsheet</u>.



۲C	Comparing	Catch	Basin	Volume	versus	Runoff	Potential: —
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Runoff potential:	
Catch basin volume:	

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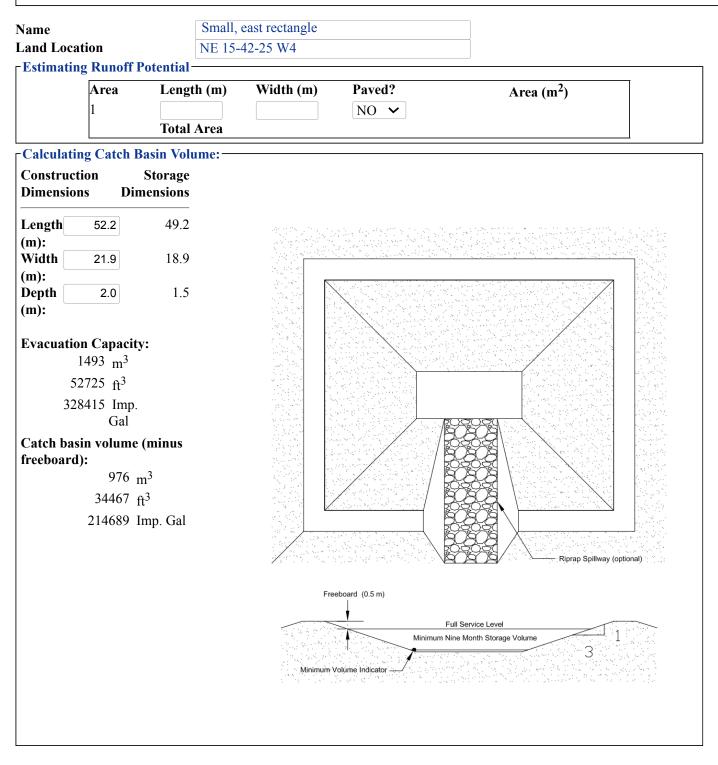
m³ 8885 m³

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The catch basin dimensions meet the design requirements in AOPA

Catch Basin Dimension Calculator

For more information on runoff control catch basin design consideration including liner options, catch basin protection, etc., check out the catch basin <u>factsheet</u>.



Comparing Catch Basin	Volume versus	Runoff Potential: —
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m³ 976 m³

Runoff potential:
Catch basin volume:

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The catch basin dimensions meet the design requirements in AOPA

Manure Spreading Agreement

This agreement is between	Morris Thalen	, manure
producer, and		

Manure receiver. Morsan Farms

Length of agreement: This agreement is valid for a time period of _____3 years_ (minimum of three years)

Legal land location	Soil type ¹	Acres suitable for manure spreading ²
N 20-42-25-W4	Black	230 acres

¹ Soil type choices: Dark brown and brown, Grey wooded, Black, Irrigated.

² Land within required setbacks from water bodies, water wells, residences, etc. is not to be included.

Other comments:

Manure producer (confined Feeding Operation) Legal Land Location_

winber 17 20 Date of signing

Signature

Print name

Corporate name(if appl)

Manure Receiver - Landowner(s)³

Date of signing

Signature

Print name

MORSAN FARMS

Corporate name(if appl)

Date of signing

Signature

Print name ³ All registered owners of land, or authorized signing authorities must sign. Corporate name(if appl)

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